4
Engineering Academy
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# GATE 2017 <br> Mechanical Engineering 

## Questions with Detailed Solutions

## AFTERNOON SESSION

## Mechanical Engineering

1. Consider a laminar flow at zero over a flat plate. The shear stress at the wall is denoted by $\tau_{\mathrm{w}}$. The axial positions $x_{1}$ and $x_{2}$ on the plate are measured from the leading edge in the direction of flow. If $\mathrm{x}_{2}>\mathrm{x}_{1}$, then
(A) $\left.\tau_{\mathrm{w}}\right|_{\mathrm{x}_{1}}=\left.\tau_{\mathrm{w}}\right|_{\mathrm{x}_{2}}=0$
(B) $\left.\tau_{\mathrm{w}}\right|_{\mathrm{x}_{1}}=\left.\tau_{\mathrm{w}}\right|_{\mathrm{x}_{2}} \neq 0$
(C) $\left.\tau_{w}\right|_{x_{1}}>\left.\tau_{w}\right|_{x_{2}}$
(D) $\left.\tau_{\mathrm{w}}\right|_{\mathrm{x}_{1}}<\left.\tau_{\mathrm{w}}\right|_{\mathrm{x}_{2}}$
2. Ans: (C)

Sol: $\tau_{\mathrm{w}}(\mathrm{x})=\frac{1}{2} \mathrm{c}_{\mathrm{fx}} \rho \mathrm{U}_{\infty}^{2}=\frac{1}{2} \times \frac{0.332}{\sqrt{\frac{\rho \mathrm{U}_{\infty} \mathrm{x}}{\mu}}} \times \rho \mathrm{U}_{\infty}^{2}$

$$
\propto \frac{1}{\sqrt{\mathrm{x}}}
$$

$\therefore \frac{\tau_{\mathrm{w}}}{\mathrm{x}_{1}}>\frac{\tau_{\mathrm{w}}}{\mathrm{x}_{2}}$
02. If a mass of moist air contained in a closed metallic vessel is heated, then its
(A) relative humidity decreases
(B) relative humidity increases
(C) specific humidity increases
(D) specific humidity decreases
02. Ans: (A)

Sol: Sensible heating process, RH decreases

03. A cantilever beam of length $L$ and flexural modulus EI is subjected to a point load P at the free end. The elastic strain energy stored in the beam due to bending (neglecting transverse shear) is
(A) $\frac{\mathrm{P}^{2} \mathrm{~L}^{3}}{6 \mathrm{EI}}$
(B) $\frac{\mathrm{P}^{2} \mathrm{~L}^{3}}{3 \mathrm{EI}}$
(C) $\frac{\mathrm{PL}^{3}}{3 \mathrm{EI}}$
(D) $\frac{\mathrm{PL}^{3}}{6 \mathrm{EI}}$
03. Ans: (A)

Sol: $\quad U=\frac{M^{2} d x}{2 E I}$

$$
\begin{aligned}
& =\int_{0}^{\ell} \frac{(P x)^{2} d x}{2 E I} \\
& =\frac{P^{2}}{2 E I}\left[\frac{x^{3}}{3}\right]_{0}^{\ell} \\
U & =\frac{P^{2} \ell^{3}}{6 E I}
\end{aligned}
$$

4. The emissive power of a blackbody is P . If its absolute temperature is doubled, the emissive power becomes
(A) 2 P
(B) 4 P
(C) 8 P
(D) 16 P

## 04. Ans: (D)

Sol: $\mathrm{E} \propto \mathrm{T}^{4}, \mathrm{~T}_{2}=2 \mathrm{~T}_{1}, \mathrm{E}_{1}=\mathrm{P}$

$$
\frac{\mathrm{E}_{1}}{\mathrm{E}_{2}}=\frac{\mathrm{T}_{1}^{4}}{\mathrm{~T}_{2}^{4}}
$$

$$
\frac{\mathrm{E}_{1}}{\mathrm{E}_{2}}=\frac{\left(\mathrm{T}_{1}\right)^{4}}{\left(2 \mathrm{~T}_{1}\right)^{4}}
$$

$$
\frac{\mathrm{E}_{1}}{\mathrm{E}_{2}}=\frac{\mathrm{T}_{1}^{4}}{16 \mathrm{~T}_{1}^{4}}
$$

$$
\mathrm{E}_{2}=16 \mathrm{E}_{1}
$$

$$
\mathrm{E}_{2}=16 \mathrm{P}
$$

5. For a single server with Poisson arrival and exponential service time, the arrival rate is 12 per hour. Which one of the following rates will provide a steady state finite queue length?
(A) 6 per hour
(B) 10 per hour
(C) 12 per hour
(D) 24 per hour
6. Ans: (D)

Sol: Arrival rate $=\lambda=12 \mathrm{hr}^{-1}$
For finite Que length departure rate must be greater than arrival rate. ( $\mu>\lambda$ )
$\therefore \mu=24 \mathrm{hr}^{-1}$
06. A mass $m$ of a perfect gas at pressure $p_{1}$ and volume $V_{1}$ undergoes an isothermal process. The final pressure is $\mathrm{p}_{2}$ and volume is $\mathrm{V}_{2}$. The work done on the system is considered positive. If R is the gas constant and T is the temperature, then the work done in the process is
(A) $\mathrm{p}_{1} \mathrm{~V}_{1} \ln \frac{\mathrm{~V}_{2}}{\mathrm{~V}_{1}}$
(B) $-\mathrm{p}_{1} \mathrm{~V}_{1} \ln \frac{\mathrm{p}_{1}}{\mathrm{p}_{2}}$
(C) $R T \ell \frac{V_{2}}{V_{1}}$
(D) $-\mathrm{mRT} \ell \frac{\mathrm{p}_{2}}{\mathrm{p}_{1}}$

## 06. Ans: (B)

Sol: $\mathrm{P}_{1} \mathrm{~V}_{1}=\mathrm{P}_{2} \mathrm{~V}_{2}$ (isothermal)
$\frac{\mathrm{P}_{1}}{\mathrm{P}_{2}}=\frac{\mathrm{V}_{2}}{\mathrm{~V}_{1}}$
Isothermal work $=-P_{1} V_{1} \ln \frac{V_{2}}{V_{1}}=-P_{1} V_{1} \ln \frac{P_{1}}{P_{2}}$
07. The crystal structure of aluminium is
(A) body -centred cubic
(B) face - centred cubic
(C) close - packed hexagonal
(D) body - centred tetragonal
07. Ans: (B)
08. The Laplace transform of te ${ }^{t}$ is
(A) $\frac{\mathrm{s}}{(\mathrm{s}+1)^{2}}$
(B) $\frac{1}{(s-1)^{2}}$
(C) $\frac{1}{(s+1)^{2}}$
(D) $\frac{\mathrm{s}}{\mathrm{s}-1}$

## 08. Ans: (B)

Sol: We know that, $L(t)=\frac{1}{\mathrm{~s}^{2}}$
By first shifting property,

$$
\mathrm{L}\left(\mathrm{te}^{\mathrm{t}}\right)=\frac{1}{(\mathrm{~s}-1)^{2}}
$$

9. The determinant of a $2 \times 2$ matrix is 50 . If one eigenvalue of the matrix is 10 , the other eigenvalue is $\qquad$ .

## 09. Ans: 5

Sol: Let, $\lambda_{1}, \lambda_{2}$ be two eigen values of A
Let, $\lambda_{1}=10$.
Given that, $\operatorname{det}(\mathrm{A})=50$
$\Rightarrow \lambda_{1} \lambda_{2}=50(\because$ Product of Eigen values of $A=\operatorname{det}(\mathrm{A})]$
$\Rightarrow 10 \lambda_{2}=50$
$\Rightarrow \lambda_{2}=5$
10. It is desired to make a product having T-shaped cross - section from a rectangular aluminium block. Which one of the following processes is expected to provide the highest strength of the product?
(A) Welding
(B) Casting
(C) Metal forming
(D) Machining
10. Ans: (C)

Sol: Metal forming gives grain orientation and fine grains. Hence strength is high.

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11. The heat loss from a fin is 6 W . The effectiveness of the fin are 3 and 0.75 , respectively. The heat loss (in W) from the fin, keeping the entire fin surface at base temperature, is $\qquad$

## 11. Ans: 8

Sol: $\mathrm{Q}_{\mathrm{act}}=6 \mathrm{~W}$
Effectiveness $(\epsilon)=3$
Efficiency $(\eta)=0.75$
Entire fin is maintained at base temperature means $\mathrm{Q}_{\text {max }}$
$\eta=\frac{\mathrm{Q}_{\text {act }}}{\mathrm{Q}_{\text {max }}}$
$0.75=\frac{6}{\mathrm{Q}_{\max }}$
$\mathrm{Q}_{\text {max }}=\frac{6}{0.75}$
$\mathrm{Q}_{\text {max }}=8 \mathrm{~W}$
12. Given the atomic weight of Fe is 56 and that of C is 12 , the weight percentage of carbon in cementite $\left(\mathrm{Fe}_{3} \mathrm{C}\right)$ is $\qquad$
12. Ans: 6.67

Sol: The percentage of carbon $\left(\mathrm{Fe}_{3} \mathrm{C}\right)=\frac{12}{56 \times 3+12 \times 1} \times 100=6.67 \%$
13. In a slider-crank mechanism, the lengths of the crank and the connecting rod are 100 mm and 160 mm , respectively. The crank is rotating with an angular velocity of $10 \mathrm{radian} / \mathrm{s}$ counterclockwise. The magnitude of linear velocity (in $\mathrm{m} / \mathrm{s}$ ) of the piston at the instant corresponding to the configuration shown in the figure is $\qquad$


## 13. Ans: 1

## Sol:



(Velocity Diagram)
From the velocity diagram when crank is perpendicular to the line of stroke, the velocity of slider $=$ velocity of crank and angular velocity of connecting rod is zero.
$\omega_{2}=10 \mathrm{rad} / \mathrm{s}$
At this position, i.e. crank angle $\theta=90^{\circ} \quad V_{\text {slider }}=r \omega_{2}=10 \times 100 \mathrm{~mm} / \mathrm{s}$
$\therefore$ Slider velocity $=1 \mathrm{~m} / \mathrm{s}$
14. A mass m is attached to two identical springs having spring constant k as shown in figure. The natural frequency $\omega$ of this single degree of freedom system is

(A) $\sqrt{\frac{2 \mathrm{k}}{\mathrm{m}}}$
(B) $\sqrt{\frac{\mathrm{k}}{\mathrm{m}}}$
(C) $\sqrt{\frac{\mathrm{k}}{2 \mathrm{~m}}}$
(D) $\sqrt{\frac{4 \mathrm{k}}{\mathrm{m}}}$
14. Ans: (A)

Sol: Springs are in parallel connections

$$
\begin{aligned}
& \mathrm{k}_{\mathrm{eq}}=\mathrm{k}+\mathrm{k}=2 \mathrm{k} \\
& \omega_{\mathrm{n}}=\sqrt{\frac{\mathrm{k}_{\mathrm{eq}}}{\mathrm{~m}_{\mathrm{eq}}}}=\sqrt{\frac{2 \mathrm{k}}{\mathrm{~m}}} \mathrm{rad} / \mathrm{sec}
\end{aligned}
$$

15. Which one of the following statements is TRUE?
(A) Both Pelton and Francis turbines are impulse turbines.
(B) Francis turbine is a reaction turbine but Kaplan turbine is an impulse turbine.
(C) Francis turbine is an axial-flow reaction turbine.
(D) Kaplan turbine is an axial-flow reaction turbine.
16. Ans: (D)
17. The state of stress at a point is $\sigma_{x}=\sigma_{y}=\sigma_{z}=\tau_{x z}=\tau_{\mathrm{zx}}=\tau_{\mathrm{yz}}=\tau_{\mathrm{zy}}=0$ and $\tau_{\mathrm{xy}}=\tau_{\mathrm{yx}}=50 \mathrm{MPa}$. The maximum normal stress (in MPa) at that point is $\qquad$
18. Ans: 50

Sol: The state of stress is pure shear
Hence, $\sigma_{1}=-\sigma_{2}=\tau$
$\therefore \sigma_{\text {max }}=50 \mathrm{MPa}$
17. Which one of the following statements is TRUE for the ultrasonic machining (USM) process?
(A) In USM, the tool vibrates at subsonic frequency.
(B) USM does not employ magnetostrictive transducer.
(C) USM is an excellent process for machining ductile materials.
(D) USM often uses a slurry comprising abrasive-particles and water.

## 17. Ans: (D)

Sol: In USM vibration is in ultrasonic range, it uses piezoelectric (or) magnetostrictive transducer for producing high frequency vibrations and it is used only for brittle materials.
18. For a loaded cantilever beam of uniform cross-section, the bending moment (in N-mm) along the length is $M(x)=5 x^{2}+10 x$, where $x$ is the distance (in mm) measured from the free end of the beam. The magnitude of shear force (in N ) in the cross-section at $\mathrm{x}=10 \mathrm{~mm}$ is $\qquad$
18. Ans: 110

Sol: $M(x)=5 x^{2}+10 x$
Shear force $F=\frac{d M}{d x}=10 x+10=10 \times 10+10=110 N$
19. The divergence of the vector $-\mathrm{yi}+\mathrm{xj}$ is $\qquad$
19. Ans: 0

Sol: $\operatorname{div}(-y i+x j)=\frac{\partial}{\partial x}(-y)+\frac{\partial}{\partial y}(x)=0$
20. The standard deviation of linear dimensions P and Q are $3 \mu \mathrm{~m}$ and $4 \mu \mathrm{~m}$, respectively. When assembled, the standard deviation (in $\mu \mathrm{m}$ ) of the following linear dimension $(P+Q)$ is $\qquad$
20. Ans: 5

Sol: Variance $(\mathrm{P}+\mathrm{Q})=$ variance $(\mathrm{P})+\operatorname{variance}(\mathrm{Q})$
Variance $(\mathrm{P}+\mathrm{Q})=3^{2}+4^{2}$

$$
\sigma^{2}=25
$$

Standard deviation $(P+Q)=\sqrt{25}=5 \mu \mathrm{~m}$
21. A machine component made of a ductile material is subjected to a variable loading with $\sigma_{\min }=$ -50 MPa and $\sigma_{\max }=50 \mathrm{MPa}$. If the corrected endurance limit and the yield strength for the material are $\sigma_{e}^{\prime}=100 \mathrm{MP}$ and $\sigma_{y}=300 \mathrm{MPa}$, respectively, the factor of safety is $\qquad$
21. Ans: 2

Sol: $\sigma_{\min }=-50 \mathrm{MPa}, \quad \sigma_{\max }=50 \mathrm{MPa}$,

$$
\mathrm{s}_{\mathrm{e}}=100 \mathrm{MPa}, \quad \mathrm{~s}_{\mathrm{yt}}=300 \mathrm{MPa}
$$

The stress is completely reversed stress and mean stress, $\sigma_{\mathrm{m}}=0$ and stress amplitude. $\sigma_{\mathrm{a}}=50 \mathrm{MPa}$.

$$
\begin{aligned}
& \sigma_{\mathrm{a}}=\frac{\mathrm{S}_{\mathrm{e}}}{\mathrm{FS}} \\
& 50=\frac{100}{\mathrm{FS}} \Rightarrow \mathrm{~F} . \mathrm{S}=2
\end{aligned}
$$

22. Two coins are tossed simultaneously. The probability (upto two decimal points accuracy) of getting at least one head is $\qquad$

## 22. Ans: 0.75

Sol: Sample space $=\{$ HH, HT, TH, TT $\}$
Total cases $=4$
Favourable cases for atleast one head $=3$
$\therefore$ Required Probability, $\mathrm{P}=\frac{3}{4}=0.75$
23. A sample of 15 data is as follows; $17,18,17,17,13,18,5,5,6,7,8,9,20,17,3$. The mode of the data is
(A) 4
(B) 13
(C) 17
(D) 20
23. Ans: (C)

Sol: In sample, the mode is defined as the sample point which occur maximum number of times. In the given sample, 17 occurs maximum number of times.
$\therefore$ Mode $=17$
24. For the stability of a floating body the
(A) centre of buoyancy must coincide with the centre of gravity
(B) centre of buoyancy must be above the centre of gravity
(C) centre of gravity must be above the centre of buoyancy
(D) metacentre must be above the centre of gravity

## 24. Ans: (D)

Sol: For stability of floating bodies $\mathrm{GM}>0$ or M must be above G .
25. A steel bar is held by two fixed supports as shown in the figure and is subjected to an increase of temperature $\Delta \mathrm{T}=100^{\circ} \mathrm{C}$. If the coefficient of thermal expansion and Young's modulus of elasticity of steel are $11 \times 10^{-6} /{ }^{\circ} \mathrm{C}$ and 200 GPa , respectively, the magnitude of thermal stress (in MPa) induced in the bar is $\qquad$

25. Ans: 220

Sol: Temperature increase, $\mathrm{T}=100^{\circ} \mathrm{C}$
Young's modulus of elasticity, $\mathrm{E}=200 \times 10^{3} \mathrm{MPa}$
Coefficient of thermal expansion, $\alpha=11 \times 10^{-6} /{ }^{\circ} \mathrm{C}$
Thermal stress, $\sigma_{t}=(\alpha t) E$

$$
=\left(11 \times 10^{-6}\right)(100)\left(200 \times 10^{3}\right)=220 \mathrm{MPa}
$$

26. Maximize $\mathrm{Z}=5 \mathrm{x}_{1}+3 \mathrm{x}_{2}$
subject to $\mathrm{x}_{1}+2 \mathrm{x}_{2} \leq 10, \quad \mathrm{x}_{1}-\mathrm{x}_{2} \leq 8, \quad \mathrm{x}_{1}, \mathrm{x}_{2} \geq 0$
In the starting simplex tableau, $\mathrm{x}_{1}$ and $\mathrm{x}_{2}$ are non-basic variables and the value of Z is zero. The value of Z in the next simplex tableau is $\qquad$
27. Ans: 40

Sol: $\operatorname{Max} \mathrm{z}=5 \mathrm{x}_{1}+3 \mathrm{x}_{2}$
Subject to $x_{1}+2 x_{2} \leq 10, x_{1}-x_{2} \leq 8, \quad x_{1}, x_{2} \geq 0$

$$
\begin{gathered}
\mathrm{x}_{1}+2 \mathrm{x}_{2}+\mathrm{s}_{1}=10 \\
\mathrm{x}_{1}-\mathrm{x}_{2}+\mathrm{s}_{2}=8
\end{gathered}
$$

| $\mathrm{C}_{\mathrm{j}} \rightarrow$ | 5 | 3 | 0 | 0 | $\mathrm{B}_{0}$ | Min ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SV $\downarrow$ | $\mathrm{x}_{1}$ | $\mathrm{X}_{2}$ | $\mathrm{S}_{1}$ | $\mathrm{S}_{2}$ |  |  |
| $0 \mathrm{~S}_{1}$ | 1 | 2 | 1 | 0 | 10 | 10/1 |
| $0 \mathrm{~S}_{2}$ | 1 (PE) | -1 | 0 | 1 | 8 | 8/1 $\boldsymbol{\rightarrow} \mathbf{L V}$ |
| $\mathrm{Z}_{\mathrm{j}}$ | 0 | 0 | 0 | 0 | 0 |  |
| $\mathrm{C}_{\mathrm{j}}-\mathrm{Z}_{\mathrm{j}}$ | 5 | 3 | 0 | 0 |  |  |
|  | $\uparrow(\mathrm{EV})$ |  |  |  |  |  |
| $0 \mathrm{~S}_{1}$ |  |  |  |  |  |  |
| $5 \mathrm{x}_{1}$ | 1 | -1 | 0 | 1 | 8 |  |
|  |  | Z value |  |  | 40 |  |

No need to calculate other values to save time.

$$
\therefore \mathrm{Z}_{\max }=40
$$

27. A calorically perfect gas (specific heat at constant pressure $1000 \mathrm{~J} / \mathrm{kgK}$ ) enters and leaves a gas turbine with the same velocity. The temperatures of the gas at turbine entry and exit are 1100 K and 400 K , respectively. The power produced is 4.6 MW and heat escapes at the rate of $300 \mathrm{~kJ} / \mathrm{s}$ through the turbine casing. The mass flow rate of the gas (in $\mathrm{kg} / \mathrm{s}$ ) through the turbine is
(A) 6.14
(B) 7.00
(C) 7.50
(D) 8.00
28. Ans: (B)

Sol: $\mathrm{C}_{\mathrm{p}}=1000 \mathrm{~J} / \mathrm{kgK}=1 \mathrm{~kJ} / \mathrm{kgK}$
$V_{1}=V_{2}$
$\mathrm{T}_{1}=1100 \mathrm{~K}, \mathrm{~T}_{2}=400 \mathrm{~K}$
Power $=4600 \mathrm{~kW}$
Heat loss from turbine casing $=\dot{\mathrm{Q}}=300 \mathrm{~kW}$
Mass flow rate $=\dot{\mathrm{m}}(\mathrm{kg} / \mathrm{sec})$
Apply SFEE
$\dot{\mathrm{m}}_{1}+\dot{\mathrm{Q}}=\dot{\mathrm{m}} \mathrm{h}_{2}+\dot{\mathrm{W}}$
$\dot{\mathrm{m}}\left(\mathrm{h}_{1}-\mathrm{h}_{2}\right)=\dot{\mathrm{W}}-\dot{\mathrm{Q}} \Rightarrow \dot{\mathrm{m}}_{\mathrm{p}}\left(\mathrm{T}_{1}-\mathrm{T}_{2}\right)=\dot{\mathrm{W}}-\dot{\mathrm{Q}}$
$\dot{\mathrm{m}}=\frac{\dot{\mathrm{W}}-\dot{\mathrm{Q}}}{\mathrm{C}_{\mathrm{p}}\left(\mathrm{T}_{1}-\mathrm{T}_{2}\right)}=\frac{4600-300}{1(1100-400)}=7 \mathrm{~kg} / \mathrm{sec}$


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28. The volume and temperature of air (assumed to be an ideal gas) in a closed vessel is $2.87 \mathrm{~m}^{3}$ and 300 K , respectively. The gauge pressure indicated by manometer fitted to the wall of the vessel is 0.5 bar. If the gas constant of air is $\mathrm{R}=287 \mathrm{~J} / \mathrm{kgK}$ and the atmospheric pressure is 1 bar, the mass of air (in kg ) in the vessel is
(A) 1.67
(B) 3.33
(C) 5.00
(D) 6.66
28. Ans: (C)

Sol: $\mathrm{V}_{1}=2.87 \mathrm{~m}^{3}$
$\mathrm{T}_{1}=300 \mathrm{~K}$
$\mathrm{P}_{\mathrm{abs}}=\mathrm{P}_{\mathrm{atm}}+\mathrm{P}_{\text {gauge }}$
$\mathrm{P}_{\text {abs }}=\mathrm{P}_{1}=1+0.5=1.5 \mathrm{bar}=150 \mathrm{kPa}$
$\mathrm{R}=0.287 \mathrm{~kJ} / \mathrm{kgK}$
$\mathrm{m}=\frac{\mathrm{P}_{1} \mathrm{~V}_{1}}{\mathrm{RT}_{1}}=\frac{150 \times 2.87}{0.287 \times 300}=5 \mathrm{~kg}$
29. A cylindrical pin of $25_{+0.010}^{+0.020} \mathrm{~mm}$ diameter is electroplated. Plating thickness is $2.0^{ \pm 0.005} \mathrm{~mm}$. Neglecting the gauge tolerance, the diameter (in mm, up to 3 decimal points accuracy) of the GO ring gauge to inspect the plated pin is $\qquad$
29. Ans: 29.03 mm

Sol:


Pin $=$ shaft $=25_{+0.01}^{+0.02}$
Plating thickness $=2 \pm 0.005 \mathrm{~mm}$
Go gauge size $\rightarrow$ Maximum material limit of shaft of shaft $\rightarrow \mathrm{H}$. limit of shaft
H. Limit of shaft after plating $=25.02+2 \times 2.005=29.03 \mathrm{~mm}$

Go ring size $=29.03 \mathrm{~mm}$
30. In a counter-flow heat exchanger, water is heated at the rate of $1.5 \mathrm{~kg} / \mathrm{s}$ from $40^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}$ by an oil entering at $120^{\circ} \mathrm{C}$ and leaving at $60^{\circ} \mathrm{C}$. The specific heats of water and oil are $4.2 \mathrm{~kJ} / \mathrm{kgK}$ and $2 \mathrm{~kJ} / \mathrm{kgK}$, respectively. The overall heat transfer coefficient is $400 \mathrm{~W} / \mathrm{m}^{2} \mathrm{~K}$. The required heat transfer surface are (in $\mathrm{m}^{2}$ ) is
(A) 0.104
(B) 0.022
(C) 10.4
(D) 21.84
30. Ans: (D)

## Sol: Cold fluid

$\mathrm{T}_{\mathrm{c} 1}=40^{\circ} \mathrm{C}$
$\mathrm{T}_{\mathrm{c} 2}=80^{\circ} \mathrm{C}$
$\dot{\mathrm{m}}_{\mathrm{c}}=1.5 \mathrm{~kg} / \mathrm{s}$
$\mathrm{c}_{\mathrm{c}}=4.2 \mathrm{~kJ} / \mathrm{kgK}$


## Hot fluid

$\mathrm{T}_{\mathrm{h} 1}=120^{\circ} \mathrm{C}$
$\mathrm{T}_{\mathrm{h} 2}=60^{\circ} \mathrm{C}$
$c_{\mathrm{h}}=2 \mathrm{~kJ} / \mathrm{kgK}$

## Counter flow

$\Delta \mathrm{T}_{1}=\mathrm{T}_{\mathrm{h} 1}-\mathrm{T}_{\mathrm{c} 2}$
$\Delta \mathrm{T}_{1}=120-80$
$\Delta \mathrm{T}_{1}=40^{\circ} \mathrm{C}$
$\Delta \mathrm{T}_{2}=\mathrm{T}_{\mathrm{h} 2}-\mathrm{T}_{\mathrm{c} 1}$
$\Delta \mathrm{T}_{2}=60-40$
$\Delta \mathrm{T}_{2}=20$

$$
\mathrm{LMTD}=\frac{\Delta \mathrm{T}_{1}-\Delta \mathrm{T}_{2}}{\ln \left(\frac{\Delta \mathrm{~T}_{1}}{\Delta \mathrm{~T}_{2}}\right)}=\frac{40-20}{\ln \left(\frac{40}{20}\right)}
$$

LMTD $=28.854^{\circ} \mathrm{C}$

$$
\begin{aligned}
\mathrm{Q}=\mathrm{m}_{\mathrm{c}} \mathrm{C}_{\mathrm{c}}\left(\mathrm{~T}_{\mathrm{C}_{2}}-\mathrm{T}_{\mathrm{C}_{1}}\right) & =\mathrm{UA}(\mathrm{LMTD}) \\
1.5 \times 4.2 \times 10^{3} \times(80-40) & =400 \times \mathrm{A} \times 28.85 \\
\mathrm{~A} & =21.84 \mathrm{~m}^{2}
\end{aligned}
$$

31. Block 2 slides outward on link 1 at a uniform velocity of $6 \mathrm{~m} / \mathrm{s}$ as shown in the figure. Link 1 is rotating at a constant angular velocity of 20 radian/s counterclockwise. The magnitude of the total acceleration (in $\mathrm{m} / \mathrm{s}^{2}$ ) of point P of the block with respect to fixed point O is $\qquad$

32. Ans: 243.3

Sol: $\mathrm{r}=100 \mathrm{~mm}=0.1 \mathrm{~m}$
Uniform angular velocity $=\omega=20 \mathrm{rad} / \mathrm{s}$
Angular acceleration, $\alpha=0$
Uniform sliding velocity $=V_{s}=6 \mathrm{~m} / \mathrm{s}$
$\therefore$ sliding acceleration $\mathrm{f}^{\mathrm{s}}=0$


Coriolis acceleration, $\mathrm{f}^{\mathrm{c}}=2 \mathrm{~V} \omega=2 \times 6 \times 20$

$$
=240 \mathrm{~m} / \mathrm{sec}^{2} \perp l \mathrm{lr} \text { to OP }
$$

Centripetal acceleration $=\mathrm{r} \omega^{2}=0.1 \times 20^{2}$

$$
=40 \mathrm{~m} / \mathrm{sec}^{2} \text { towards the center of rotation }
$$

Resultant acceleration $=\sqrt{\left(\mathrm{f}^{\mathrm{c}}\right)^{2}+\left(\mathrm{f}^{\text {cor }}\right)^{2}}=\sqrt{40^{2}+240^{2}}=243.3 \mathrm{~m} / \mathrm{s}^{2}$
32. A strip of 120 mm width and 8 mm thickness is rolled between two 300 mm -diameter rolls to get a strip of 120 mm width and 7.2 mm thickness. The speed of the strip at the exit is $30 \mathrm{~m} / \mathrm{min}$. There is no front or back tension. Assuming uniform roll pressure of 200 MPa in the roll bite and $100 \%$ mechanical efficiency, the minimum total power (in kW ) required to drive the two rolls is $\qquad$
32. Ans: 9.58

Sol: $b=120 \mathrm{~mm}, \mathrm{H}_{\mathrm{o}}=8, \mathrm{H}_{1}=7.2$,
$\mathrm{R}=150, \mathrm{~V}_{1}=30, \mathrm{p}=200 \mathrm{MPa}$
$\alpha=\tan ^{-1}\left(\sqrt{\frac{\Delta \mathrm{H}}{\mathrm{R}}}\right)$
$=\tan ^{-1}\left(\sqrt{\frac{0.8}{150}}\right)=4.186^{\circ}$
$\mathrm{L}_{\mathrm{c}}=\mathrm{R} \alpha=\sqrt{\Delta \mathrm{HR}}=10.951 \mathrm{~mm}$
Area $=b \times L_{c}=120 \times 10.951=1314.1 \mathrm{~mm}^{2}$
Force $=$ Area $\times \mathrm{p}=1314.1 \times 200=262.82 \mathrm{kN}$
We know that, power for two rollers
$\mathrm{P}=2 \mathrm{~T} \omega$
$\omega=\frac{\mathrm{V}}{\mathrm{R}}=\frac{\frac{30}{60}}{0.15}=3.33 \mathrm{rad} / \mathrm{s}$
$\mathrm{T}=\mathrm{F} \times \frac{\mathrm{L}_{\mathrm{c}}}{2}=262.82 \times \frac{10.95}{2}=1438.93 \mathrm{Nm}$
Power $=2 \times 3.33 \times 1438.93=9583.33 \mathrm{~W}$
Power $=9.58 \mathrm{~kW}$

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33. A product made in two factories, P and Q is transported of two destinations, R and S . The per unit costs of transportation (in Rupees) from factories to destinations are as per the following matrix.

| Factory | Destination | S |
| :---: | :--- | :--- |
| P | 10 | 7 |
| Q | 3 | 4 |

Factory P produces 7 units and factory Q produces 9 units of the product. Each destination requires 8 units. If the north-west corner method provides the total transportation cost as X (in Rupees) and the optimized (the minimum) total transportation cost is $Y$ (in rupees), then ( $\mathrm{X}-\mathrm{Y}$ ), in rupees, is
(a) 0
(b) 15
(c) 35
(d) 105

## 33. Ans: (*)

Sol:

|  | R | S | Supply |
| :---: | :---: | :---: | :---: |
| P | $7 \quad 10$ | $\times \underline{7}$ | 7 |
| Q | $1 \quad 3$ | ${ }_{8} 4$ | 9 |
| Demand | 8 | 8 |  |

North West corner rule solution
$\mathrm{TC}_{1}=\mathrm{x}=7 \times 10+1 \times 3+8 \times 4=105$
PS evaluation by stepping stone method is
$\mathrm{PS}=+7-4+3-10=-4$
If some units are transferred to PS cost of transformation decreases by Rs.4/- for every unit transferred to PS

Construct a loop and transfer units.

| 7- 10 | $+7$ |
| :---: | :---: |
| $1+3$ | - ${ }_{8} 4$ |

In negative corners least quantity is 7 add it to positive corners and deduct it from negative corners

|  | 10 |  | 7 |
| :---: | :--- | :--- | :--- |
|  | 7 | 7 |  |
| 8 | 3 | 1 | 4 |
|  |  |  |  |

Optimal transport cost $=y=7 \times 7+1 \times 4+8 \times 3$

$$
\begin{aligned}
&=49+4+24=77 \\
& \Rightarrow \mathrm{x}-\mathrm{y}=105-77=28
\end{aligned}
$$

34. The arrangement shown in the figure measures the velocity $V$ of a gas of density $1 \mathrm{~kg} / \mathrm{m}^{3}$ flowing through a pipe. The acceleration due to gravity is $9.81 \mathrm{~m} / \mathrm{s}^{2}$. If the manometric fluid is water (density $1000 \mathrm{~kg} / \mathrm{m}^{3}$ ) and the velocity V is $20 \mathrm{~m} / \mathrm{s}$, the differential head h (in mm ) between the two arms of the manometer is $\qquad$

35. Ans: 20.4

Sol: $\mathrm{V}=\sqrt{2 \mathrm{gh}}=\sqrt{2 \mathrm{gx}\left(\frac{\rho_{\mathrm{m}}}{\rho}-1\right)}$
$\therefore x=\frac{\mathrm{V}^{2}}{2 \mathrm{~g}\left(\frac{\rho_{\mathrm{m}}}{\rho}-1\right)}=\frac{20^{2}}{2 \times 9.81 \times\left(\frac{1000}{1}-1\right)}$
$=20.4 \mathrm{~mm}$
35. A 60 mm - diameter water jet strikes a plate containing a hole of 40 mm diameter as shown in the figure. Part of the jet passes through the hole horizontally, and the remaining is deflected vertically. The density of water is $1000 \mathrm{~kg} / \mathrm{m}^{3}$. If velocities are as indicated in the figure, the magnitude of horizontal force (in N ) required to hold the plate is

35. Ans: $\mathbf{6 2 8 . 3}$

Sol: $F=\rho\left(A_{1}-A_{2}\right) V^{2}$

$$
\begin{aligned}
& =1000 \times \frac{\pi}{4} \times\left(0.06^{2}-0.04^{2}\right) \times 20^{2} \\
& =628.3 \mathrm{~N}
\end{aligned}
$$

36. One kg of an ideal gas (gas constant $\mathrm{R}=287 \mathrm{~J} / \mathrm{kg} . \mathrm{K}$ ) undergoes an irreversible process from state-I ( $1 \mathrm{bar}, 300 \mathrm{~K}$ ) to state-2 $(2 \mathrm{bar}, 300 \mathrm{~K})$. The change in specific entropy $\left(\mathrm{s}_{2}-\mathrm{s}_{1}\right)$ of the gas (in $\mathrm{J} / \mathrm{kg} . \mathrm{K})$ in the process is
37. Ans: -198.93

Sol: $m=1 \mathrm{~kg}$
$\mathrm{R}=287 \mathrm{~J} / \mathrm{kgK}$
$\mathrm{P}_{1}=1 \mathrm{bar}$,
$\mathrm{P}_{2}=2 \mathrm{bar}$,
$\mathrm{T}_{1}=300 \mathrm{~K}$,
$\mathrm{T}_{2}=300 \mathrm{~K}$,
$\mathrm{T}_{1}=\mathrm{T}_{2}$ isothermal process
$\mathrm{S}_{2}-\mathrm{S}_{1}=\mathrm{m}\left(\mathrm{C}_{\mathrm{p}} \ln \frac{\mathrm{T}_{2}}{\mathrm{~T}_{1}}-\mathrm{R} \ln \frac{\mathrm{P}_{2}}{\mathrm{P}_{1}}\right)$
$=m R \ell \frac{\mathrm{P}_{1}}{\mathrm{P}_{2}}$

$$
=1 \times 287 \ln \frac{1}{2}=-198.93 \mathrm{~J} / \mathrm{K}
$$

37. The rod PQ of length $L=\sqrt{2} \mathrm{~m}$, and uniformly distributed mass of $M=10 \mathrm{~kg}$, is released from rest at the position shown in the figure. The ends slide along the frictionless faces OP and OQ. Assume acceleration due to gravity, $g=10 \mathrm{~m} / \mathrm{s}^{2}$. The mass moment of inertia of the rod about its centre of mass and an axis perpendicular to the plane of the figure is $\left(\mathrm{ML}^{2} / 12\right)$. At this instant, the magnitude of angular acceleration (in radian $/ \mathrm{s}^{2}$ ) of the rod is $\qquad$

38. Ans: 7.5

Sol: Given
$\mathrm{L}=\sqrt{2} \mathrm{~m}, \mathrm{~m}=10 \mathrm{~kg}$
$\mathrm{g}=10 \mathrm{~m} / \mathrm{s}^{2} \quad \mathrm{I}_{\mathrm{CG}}=\frac{\mathrm{mL}^{2}}{12}$
Angular acceleration, $\alpha=$ ?


The $\operatorname{rod} \mathrm{PQ}$ is in general plane motion while falling down.
$\mathrm{d}_{1}=\frac{\sqrt{2}}{2} \times \cos 45$
$\mathrm{d}_{1}=\frac{1}{2} \mathrm{~m}=\mathrm{d}_{2}$
$\mathrm{r}_{\mathrm{OQ}}=\sqrt{2} \times \sin 45$

$$
=1 \mathrm{~m}=\mathrm{r}_{\mathrm{OP}}
$$

$\mathrm{d}^{2}=\mathrm{d}_{1}^{2}+\left(\mathrm{r}_{\mathrm{OQ}}-\mathrm{d}_{2}\right)^{2}$
$\mathrm{d}^{2}=\left(\frac{1}{2}\right)^{2}+\left(1-\frac{1}{2}\right)^{2}$
$\mathrm{d}^{2}=2 \times\left(\frac{1}{2}\right)^{2}=\frac{1}{2} \mathrm{~m}^{2}$

Take moment about the I centre
Moment $=\mathrm{M}=\mathrm{I}_{0} \alpha$
$\mathrm{I}_{\mathrm{O}}=$ Mass moment of inertia with respect to instant centre $\mathrm{O}=\mathrm{I}_{\mathrm{CG}}+\mathrm{md}^{2}=\frac{\mathrm{m} \ell^{2}}{12}+\mathrm{md}^{2}$
$I_{o}=\frac{m}{12}(\sqrt{2})^{2}+m \times \frac{1}{2}=\frac{m}{6}+\frac{m}{2}=\frac{4 m}{6}=\frac{2 m}{3}$
$\alpha=$ Angular acceleration
$\mathrm{M}=$ moment with respect to $\mathrm{O}=\mathrm{W} \times \mathrm{d}_{1}=\mathrm{m} \times \mathrm{g} \times \mathrm{d}_{1}$
$\mathrm{m} \times \mathrm{g} \times \mathrm{d}_{1}=\frac{2 \mathrm{~m}}{3} \times \alpha$
$\Rightarrow \alpha=\frac{3}{2} \times 10 \times \frac{1}{2}=7.5 \mathrm{rad} / \mathrm{sec}^{2}$
38. In the Rankine cycle for a steam power plant the turbine entry and exit enthalpies are $2803 \mathrm{~kJ} / \mathrm{kg}$ and $1800 \mathrm{~kJ} / \mathrm{kg}$, respectively. The enthalpies of water at pump entry and exit are $121 \mathrm{~kJ} / \mathrm{kg}$ and 124 $\mathrm{kJ} / \mathrm{kg}$, respectively. The specific steam consumption (in $\mathrm{kg} / \mathrm{kW} . \mathrm{h}$ ) of the cycle is $\qquad$
38. Ans: $\mathbf{3 . 6}$

Sol: $\mathrm{W}_{\mathrm{T}}=\mathrm{h}_{1}-\mathrm{h}_{2}=2803-1800=1003 \mathrm{~kJ} / \mathrm{kg}$
$\mathrm{W}_{\mathrm{P}}=\mathrm{h}_{4}-\mathrm{h}_{3}=124-121=3 \mathrm{~kJ} / \mathrm{kg}$
$\mathrm{W}_{\mathrm{NET}}=\mathrm{W}_{\mathrm{T}}-\mathrm{W}_{\mathrm{P}}=1003-3=1000 \mathrm{~kJ} / \mathrm{kg}$
Specific steam consumption $=\frac{3600}{\mathrm{~W}_{\mathrm{T}}-\mathrm{W}_{\mathrm{p}}} \mathrm{kg} / \mathrm{kWhr}$

$$
=\frac{3600}{1000}=3.6 \mathrm{~kg} / \mathrm{kWhr}
$$

39. Consider the matrix $\mathrm{A}=\left[\begin{array}{ll}50 & 70 \\ 70 & 80\end{array}\right]$ whose eigenvectors corresponding to eigen values $\lambda_{1}$ and $\lambda_{2}$ are $x_{1}=\left[\begin{array}{c}70 \\ \lambda_{1}-50\end{array}\right]$ and $x_{2}=\left[\begin{array}{c}\lambda_{2}-80 \\ 70\end{array}\right]$, respectively. The value of $x_{1}^{T} x_{2}$ is $\qquad$
40. Ans: 0

Sol: $\quad \mathrm{x}_{1}^{\mathrm{T}} \mathrm{x}_{2}=\left[\begin{array}{ll}70 & \lambda_{1}-50\end{array}\right]\left[\begin{array}{c}\lambda_{2}-80 \\ 70\end{array}\right]$

$$
\begin{aligned}
& =\left[70\left(\lambda_{2}-80\right)+\left(\lambda_{1}-50\right) 70\right] \\
& =\left[70\left(\lambda_{1}+\lambda_{2}\right)-70(80+50)\right] \\
& =[70(50+80)-70(50+80)] \quad\left[\because \lambda_{1}+\lambda_{2}=\text { trace of } \mathrm{A}=50+80\right] \\
& =[0]=\mathrm{O}
\end{aligned}
$$

40. During the turning of a 20 mm -diameter steel bar at a spindle speed of 400 rpm , a tool life of 20 minute is obtained. When the same bar is turned at 200 rpm , the tool life becomes 60 minute. Assume that Taylor's tool life equation is valid. When the bar is turned at 300 rpm , the tool life (in minute) is approximately
(A) 25
(B) 32
(C) 40
(D) 50

## 40. Ans (B)

Sol: $\mathrm{D}=20 \mathrm{~mm}, \quad \mathrm{~N}_{1}=400 \mathrm{rpm}=\mathrm{V}_{1}, \quad \mathrm{~T}_{1}=20 \mathrm{~min}$
$\mathrm{N}_{2}=200 \mathrm{rpm}=\mathrm{V}_{2}, \quad \mathrm{~T}_{2}=60 \mathrm{~min}$,
$\mathrm{N}_{3}=300 \mathrm{rpm}=\mathrm{V}_{3}, \quad \mathrm{~T}_{3}=$ ?
$\mathrm{V}_{1} \mathrm{~T}_{1}{ }^{\mathrm{n}}=\mathrm{V}_{2} \mathrm{~T}_{2}{ }^{\mathrm{n}}$
$\left(\frac{\mathrm{T}_{1}}{\mathrm{~T}_{2}}\right)^{\mathrm{n}}=\frac{\mathrm{V}_{2}}{\mathrm{~V}_{1}}$
$\mathrm{n}=\frac{\ln \left(\frac{\mathrm{V}_{2}}{\mathrm{~V}_{1}}\right)}{\ln \left(\frac{\mathrm{T}_{1}}{\mathrm{~T}_{2}}\right)}=\frac{\ln \left(\frac{200}{400}\right)}{\ln \left(\frac{20}{60}\right)}=0.631$
$\mathrm{V}_{3} \mathrm{~T}_{3}{ }^{\mathrm{n}}=\mathrm{V}_{1} \mathrm{~T}_{1}{ }^{\mathrm{n}}$
$\mathrm{T}_{3}=\mathrm{T}_{1}\left(\frac{\mathrm{~V}_{1}}{\mathrm{~V}_{3}}\right)^{\frac{1}{n}}$
$=20\left(\frac{400}{300}\right)^{\frac{1}{0.631}}=31.557=32 \mathrm{~min}$

41. A single-plate clutch has a friction disc with inner and outer radii of 20 mm and 40 mm , respectively. The friction lining in the disc is made in such a way that the coefficient of friction $\mu$ varies radially as $\mu=0.01 \mathrm{r}$, where r is in mm . The clutch needs to transmit a friction torque of $18.85 \mathrm{kN} . \mathrm{mm}$. As per uniform pressure theory, the pressure (in MPa) on the disc is $\qquad$
41. Ans: 0.5

Sol: $\mathrm{r}_{1}=40 \mathrm{~mm}, \quad \mathrm{r}_{2}=20 \mathrm{~mm}, \quad \mu=0.01 \mathrm{r}$,
$\mathrm{T}=18.85 \mathrm{kN}-\mathrm{mm}$,
$\mathrm{p}=\mathrm{c}$
Torque, $\delta \mathrm{T}=\mu \mathrm{P} \times 2 \pi \mathrm{rdr} \times \mathrm{r}$
$\mathrm{T}=\mathrm{P} \times 2 \pi \int_{\mathrm{r}_{2}}^{\mathrm{r}_{1}} \mu \mathrm{r}^{2} \mathrm{dr}$

$$
\begin{aligned}
& =\mathrm{P} \times 2 \pi \times 0.01 \times \int_{\mathrm{r}_{2}}^{\mathrm{r}_{1}} \mathrm{r}^{3} \mathrm{dr} \\
& =\mathrm{P} \times 2 \pi \times 0.01 \times\left[\frac{\mathrm{r}_{1}^{4}-\mathrm{r}_{2}^{4}}{4}\right]
\end{aligned}
$$

$$
18.85 \times 10^{3}=\mathrm{P} \times 2 \pi \times 0.01 \times\left[\frac{40^{4}-20^{4}}{4}\right]
$$

$$
\Rightarrow \mathrm{P}=0.5 \mathrm{~N} / \mathrm{mm}^{2}
$$

42. For the laminar flow of water over a sphere, the drag coefficient $C_{F}$ is defined as $C_{F}=F /\left(\rho U^{2} D^{2}\right)$, where $F$ is the drag force, $\rho$ is the fluid density, $U$ is the fluid velocity and $D$ is the diameter of the sphere. The density of water is $10000 \mathrm{~kg} / \mathrm{m}^{3}$. When the diameter of the sphere is 100 mm and the fluid velocity is $2 \mathrm{~m} / \mathrm{s}$, the drag coefficient is 0.5 . If water now flows over another sphere of diameter 200 mm under dynamically similar conditions, the drag force (in N ) on this sphere is
43. Ans: 20

Sol: For dynamic similarity
$(\operatorname{Re})_{1}=(\mathrm{Re})_{2}$
or $\left(\frac{\rho U D}{\mu}\right)_{1}=\left(\frac{\rho U D}{\mu}\right)_{2}$
$\therefore \mathrm{U}_{1} \mathrm{D}_{1}=\mathrm{U}_{2} \mathrm{D}_{2}$
In general $C_{F}=f(R e)$ hence in dynamically similar conditions $C_{F 1}=C_{F 2}$
Now, $\quad \mathrm{F}_{2}=\mathrm{C}_{\mathrm{F} 2} \rho \mathrm{U}_{2}^{2} \mathrm{D}_{2}^{2}$

$$
\begin{aligned}
& =\mathrm{C}_{\mathrm{F} 1} \rho \mathrm{U}_{1}^{2} \mathrm{D}_{1}^{2} \quad\left(\because \mathrm{C}_{\mathrm{F} 1}=\mathrm{C}_{\mathrm{F} 2} \& \mathrm{U}_{1} \mathrm{D}_{1}=\mathrm{U}_{2} \mathrm{D}_{2}\right) \\
& =0.5 \times 1000 \times 2 \times 0.1^{2} \\
& =20 \mathrm{~N}
\end{aligned}
$$

43. A helical compression spring made of a wire of circular cross-section is subjected to a compressive load. The maximum shear stress induced in the cross-section of the wire is 24 MPa . For the same compressive load, if both the wire diameter and the mean coil diameter are doubled, the maximum shear stress (in MPa) induced in the cross-section of the wire is $\qquad$
44. Ans: 6

Sol: Shear stress in helical spring is
$\tau_{\text {max }}=\frac{8 \mathrm{PD}}{\pi \mathrm{d}^{3}} \times \mathrm{k}_{\mathrm{w}}$
$\mathrm{k}_{\mathrm{w}}=$ Wahl's factor $=\frac{4 \mathrm{C}-1}{4 \mathrm{C}-4}+\frac{0.615}{\mathrm{C}}$
$\tau_{\text {max }}=24 \mathrm{MPa}$
For same load, D and d are doubled
So there is no change in $\mathrm{C}=\frac{\mathrm{D}}{\mathrm{d}}=\frac{2 \mathrm{D}}{2 \mathrm{~d}}$
$\therefore$ Wahl's factor is same

$$
\begin{aligned}
& \tau_{\max }^{\prime}=\mathrm{k}_{\mathrm{w}} \times \frac{8 \mathrm{P}(2 \mathrm{D})}{\pi(2 \mathrm{~d})^{3}} \\
& \tau_{\max }^{\prime}=\mathrm{k}_{\mathrm{w}} \times \frac{8 \mathrm{PD}}{\pi \mathrm{~d}^{3}} \times \frac{2}{8}=\frac{\tau_{\max }}{4} \\
& \tau_{\max }^{\prime}=\frac{24}{4}=6 \mathrm{MPa}
\end{aligned}
$$

44. A steel plate, connected to a fixed channel using three identical bolts $\mathrm{A}, \mathrm{B}$ and C , carries a load of 6 kN as shown in the figure. Considering the effect of direct load and moment, the magnitude of resultant shear force (in kN ) on bolt C is


All dimensions are in mm.
(A) 13
(B) 15
(C) 17
(D) 30
44. Ans: (C)

Sol:


Primary shear, load, $\mathrm{P}_{\mathrm{s}_{1}}=\frac{6}{3}=2 \mathrm{kN}$
Secondary shear, load, $\mathrm{P}_{\mathrm{s}_{1}}^{\prime}=\mathrm{kr}_{1}$

$$
=\frac{\mathrm{P} \times \mathrm{e}}{\mathrm{r}_{1}^{2}+\mathrm{r}_{2}^{2}+\mathrm{r}_{3}^{2}} \times \mathrm{r}_{1}
$$

$$
\begin{aligned}
& \mathrm{r}_{1}=\mathrm{r}_{3}=50 \& \mathrm{r}_{2}=0 \& \mathrm{e}=250 \mathrm{~mm} \\
& \therefore \mathrm{P}_{\mathrm{s}_{1}}^{\prime}= \\
& =\frac{6 \times 250}{50^{2}+0^{2}+50^{2}} \times 50 \\
& \\
& =\frac{6 \times 250}{2 \times 50^{2}} \times 56=15 \mathrm{kN}
\end{aligned}
$$

$\therefore$ Resultant load on c, $\mathrm{P}_{\mathrm{s}}=\mathrm{P}_{\mathrm{s}_{1}}+\mathrm{P}_{\mathrm{s}_{1}}^{\prime}=2+15=17 \mathrm{kN}$
45. If $f(z)=\left(x^{2}+a y^{2}\right)+i b x y$ is a complex analytic function of $z=x+i y$, where $I=\sqrt{-1}$, then
(A) $a=-1, b=-1$
(B) $a=-1, b=2$
(C) $\mathrm{a}=1, \mathrm{~b}=2$
(D) $a=2, b=2$
45. Ans: (B)

Sol: Let, $\mathrm{f}(\mathrm{z})=\left(\mathrm{x}^{2}+\mathrm{ay}{ }^{2}\right)+\mathrm{ibxy}=\mathrm{u}+\mathrm{iv}$ (say)
Where, $u=x^{2}+a y^{2}$,

$$
\mathrm{u}_{\mathrm{y}}=2 \mathrm{ay}
$$

$$
\begin{aligned}
v & =b x y \\
-v_{x} & =-b y \\
v_{y} & =b x
\end{aligned}
$$

$$
\mathrm{u}_{\mathrm{x}}=2 \mathrm{x}, \quad-\mathrm{v}_{\mathrm{x}}=-\mathrm{by}
$$

Using C-R equations, we have
$\Rightarrow \mathrm{u}_{\mathrm{x}}=\mathrm{v}_{\mathrm{y}} \quad \& \mathrm{u}_{\mathrm{y}}=-\mathrm{v}_{\mathrm{x}}$
$\Rightarrow 2 \mathrm{x}=\mathrm{bx} \& 2 \mathrm{ay}=-\mathrm{by}$
$\therefore \mathrm{b}=2, \mathrm{a}=-1$
46. Consider the differential equation $3 y^{\prime \prime}(x)+27 y(x)=0$ with initial conditions $y(0)=0$ and $y^{\prime}(0)=$ 2000. The value of $y$ at $x=1$ is $\qquad$
46. Ans: $\mathbf{3 4 . 8 9}$

Sol: Given, $3 y^{\prime \prime}(x)+27 y(x)=0, y(0)=0, y^{\prime}(0)=2000$

$$
\left(3 D^{2}+27\right) y=0
$$

The auxiliary equation is

$$
\begin{aligned}
& 3 \mathrm{D}^{2}+27=0 \\
& \Rightarrow \mathrm{D}= \pm 3 \mathrm{i}
\end{aligned}
$$

$\therefore$ The general solution is

$$
\begin{align*}
& y=c_{1} \cos 3 x+c_{2} \sin 3 x  \tag{1}\\
& \mathrm{y}^{\prime}=-3 c_{1} \sin 3 \mathrm{x}+3 \mathrm{c}_{2} \cos 3 \mathrm{x}  \tag{2}\\
& \mathrm{y}(0)=0 \Rightarrow 0=\mathrm{c}_{1} \\
& \mathrm{y}^{\prime}(0)=2000 \Rightarrow 2000=3 \mathrm{c}_{2} \\
& \Rightarrow \mathrm{c}_{2}=\frac{2000}{3}
\end{align*}
$$

$\therefore$ Substituting the values of $\mathrm{c}_{1}$ and $\mathrm{c}_{2}$ in equation (1), the particular solution is

$$
\begin{gathered}
y=\frac{2000 \sin 3 x}{3} \\
\text { At } \mathrm{x}=1, \mathrm{y}=\frac{2000 \sin 3}{3}=34.89
\end{gathered}
$$

47. The principal stresses at a point in a critical section of a machine component are $\sigma_{1}=60 \mathrm{MPa}$, $\sigma_{2}=5 \mathrm{MPa}$ and $\sigma_{3}=-40 \mathrm{Mpa}$. For the material of the component, the tensile yield strength is $\sigma_{\mathrm{y}}=$ 200 MPa . According to the maximum shear stress theory, the factor of safety is
(A) 1.67
(B) 2.00
(C) 3.60
(D) 4.00

## 47. Ans: (B)

Sol: $\sigma_{1}=60 \mathrm{MPa}, \sigma_{2}=5 \mathrm{MPa}, \sigma_{3}=-40 \mathrm{MPa}$,
$\mathrm{s}_{\mathrm{yt}}=200 \mathrm{MPa}$
According to MSST,
$\tau_{\text {max }}=\frac{\mathrm{S}_{\mathrm{yt}}}{2 \times \mathrm{FS}}$
$\frac{\sigma_{1}-\sigma_{3}}{2}=\frac{\mathrm{s}_{\mathrm{yt}}}{2 \times \mathrm{FS}}$
$\sigma_{1}-\sigma_{3}=\frac{\mathrm{s}_{\mathrm{yt}}}{\mathrm{FS}}$
$60-(-40)=\frac{200}{F S}$
$100=\frac{200}{\mathrm{FS}} \Rightarrow \mathrm{FS}=2$
48. The surface integral $\iint_{S} F$.ndS over the surface $S$ of the sphere $x^{2}+y^{-2}+z^{2}=9$, where $F=(x+y) I+$ $(x+z) j+(y+z) k$ and $n$ is the unit outward surface normal, yields $\qquad$
48. Ans: 226.08

Sol: $\quad \overrightarrow{\mathrm{F}}=(\mathrm{x}+\mathrm{y}) \overrightarrow{\mathrm{i}}+(\mathrm{x}+\mathrm{z}) \overrightarrow{\mathrm{j}}+(\mathrm{y}+\mathrm{z}) \overrightarrow{\mathrm{k}}$
$\operatorname{div} \overrightarrow{\mathrm{F}}=1+1=2$

$$
\begin{aligned}
\iint_{\mathrm{S}} \overrightarrow{\mathrm{~F}} \cdot \overrightarrow{\mathrm{n}} \mathrm{dS} & =\iiint_{\mathrm{V}} \operatorname{div} \overrightarrow{\mathrm{~F}} \mathrm{dx} d y \mathrm{dz} \quad \text { (By Gauss divergence theorem) } \\
& =\iiint 2 \mathrm{dx} d y \mathrm{dz} \\
& =2\left(\text { volume of the sphere } \mathrm{x}^{2}+\mathrm{y}^{2}+\mathrm{z}^{2}=9\right) \\
& =2 \times \frac{4}{3} \pi(3)^{3} \\
& =72 \pi=226.08
\end{aligned}
$$

49. A project starts with activity A and ends with activity F. The precedence relation and durations of the activities are as per the following table:

| Activity | Immediate predecessor | Duration (days) |
| :---: | :---: | :---: |
| A | - | 4 |
| B | A | 3 |
| C | A | 7 |
| D | B | 14 |
| E | C | 4 |
| F | D,E | 9 |

The minimum project completion time (in days) is $\qquad$
49. Ans: 30

Sol:


| Paths |  |
| :--- | :--- |
| ABDF | $4+3+14+9=30$ days |
| ACEF | $4+7+4+9=24$ days |

Longest path is critical path duration $=30$ days
50. The radius of gyration of a compound pendulum about the point of suspension is 100 mm . The distance between the point of suspension and the centre of mass is 250 mm . Considering the acceleration due to gravity as $9.81 \mathrm{~m} / \mathrm{s}^{2}$, the natural frequency (in radian $/ \mathrm{s}$ ) of the compound pendulum is $\qquad$
50. Ans: $\mathbf{1 5 . 6 6}$

Sol: Radius of gyration, $\mathrm{r}=100 \mathrm{~mm}=0.1 \mathrm{~m}, \mathrm{~L}=250 \mathrm{~mm}=0.25 \mathrm{~m}, \mathrm{~g}=9.81 \mathrm{~m} / \mathrm{sec}^{2}$ $\omega_{\mathrm{n}}=$ ?
The equation of motion is $I_{0} \ddot{\theta}+m g L \sin \theta=0$
For small value of $\theta, \sin \theta \simeq \theta$
$\therefore \omega_{\mathrm{n}}=\sqrt{\frac{\mathrm{mgL}}{\mathrm{I}_{0}}}$
$\therefore \mathrm{I}_{\mathrm{o}}=\mathrm{mr}^{2}$
$\therefore \omega_{\mathrm{n}}=\sqrt{\frac{\mathrm{mgL}}{\mathrm{mr}^{2}}}=\sqrt{\frac{\mathrm{gL}}{\mathrm{r}^{2}}}=\sqrt{\frac{9.81 \times 0.25}{0.1^{2}}} \mathrm{rad} / \mathrm{s}=15.66 \mathrm{rad} / \mathrm{s}$
51. A gear train shown in the figure consists of gears $P, Q, R$ and $S$. Gear $Q$ and gear $R$ are mounted on the same shaft. All the gears are mounted on parallel shafts and the number of teeth of $\mathrm{P}, \mathrm{Q}, \mathrm{R}$ and $S$ are $24,45,30$ and 80 , respectively. Gear $P$ is rotating at 400 rpm . The speed (in rpm) of the gear $S$ is $\qquad$

51. Ans: 120

Sol: $\quad \mathrm{N}_{\mathrm{P}}=400 \mathrm{rpm}$,
$\mathrm{N}_{\mathrm{s}}=$ ?
$\therefore \frac{\mathrm{N}_{\mathrm{P}}}{\mathrm{N}_{\mathrm{s}}}=\frac{\mathrm{T}_{\mathrm{s}}}{\mathrm{T}_{\mathrm{P}}}$
$\therefore \frac{400}{\mathrm{~N}_{\mathrm{s}}}=\frac{80}{24}$
$\therefore \mathrm{N}_{\mathrm{s}}=120 \mathrm{rpm}$
52. In an orthogonal machining with a tool of $9^{\circ}$ orthogonal rake angle, the uncut chip thickness is 0.2 mm . The chip thickness fluctuates between 0.25 mm and 0.4 mm . The ratio of the maximum shear angle to the minimum shear angle during machining is $\qquad$
52. Ans: $\mathbf{1 . 5}$

Sol: $\alpha=9^{\circ}, \mathrm{t}_{1}=0.2, \mathrm{t}_{2}=0.25$ to 0.4
$\mathrm{r}_{\text {max }}=\frac{\mathrm{t}_{1}}{\mathrm{t}_{2 \text { min }}}=\frac{0.2}{0.25}=0.8$
$\phi_{\text {max }}=\tan ^{-1}\left(\frac{r_{\text {max }} \cos \alpha}{1-r_{\text {max }} \sin \alpha}\right)=42.087$
$r_{\text {min }}=\frac{t_{1}}{t_{2 \max }}=\frac{0.2}{0.4}=0.5$
$\phi_{\text {min }}=\tan ^{-1}\left(\frac{\mathrm{r}_{\text {min }} \cos \alpha}{1-\mathrm{r}_{\text {min }} \sin \alpha}\right)=28.18$
Ratio $=\frac{\phi_{\text {max }}}{\phi_{\text {min }}}=\frac{42.087}{28.18}=1.493=1.5$
53. A rod of length 20 mm is stretched to make a rod of length 40 mm . Subsequently, it is compressed to make a rod of final length 10 mm . Consider the longitudinal tensile strain as positive and compressive strain as negative. The total true longitudinal strain in the rod is
(A) -0.5
(B) -0.69
(C) -0.75
(D) -1.0
53. Ans: (B)

Sol: $\mathrm{L}_{1}=20 \mathrm{~mm}, \mathrm{~L}_{2}=40 \mathrm{~mm}, \mathrm{~L}_{3}=10 \mathrm{~mm}$,
$\mathrm{A}_{1} \mathrm{~L}_{1}=\mathrm{A}_{2} \mathrm{~L}_{2}=\mathrm{A}_{3} \mathrm{~L}_{3}$

$$
\frac{\mathrm{A}_{1}}{\mathrm{~A}_{3}}=\frac{\mathrm{L}_{3}}{\mathrm{~L}_{1}}
$$

True strain $=\ell n\left(\frac{\mathrm{~A}_{1}}{\mathrm{~A}_{3}}\right)=\ln \left(\frac{\mathrm{L}_{3}}{\mathrm{~L}_{1}}\right)$

$$
=\ln \left(\frac{10}{20}\right)=-0.693
$$

54. A metal ball of diameter 60 mm is initially at $220^{\circ} \mathrm{C}$. The ball is suddenly cooled by an air jet of $20^{\circ} \mathrm{C}$. The heat transfer coefficient is $200 \mathrm{~W} / \mathrm{m}^{2}$. K. The specific heat, thermal conductivity and density of the metal ball are $400 \mathrm{~J} / \mathrm{kg} . \mathrm{K}, 400 \mathrm{~W} / \mathrm{m} . \mathrm{K}$ and $9000 \mathrm{~kg} / \mathrm{m}^{3}$, respectively. The ball temperature (in ${ }^{\circ} \mathrm{C}$ ) after 90 seconds will be approximately
(A) 141
(B) 163
(C) 189
(D) 210
55. Ans: (A)

Sol: Given data
$\mathrm{R}=0.03 \mathrm{~m}$
$\mathrm{T}_{0}=220^{\circ} \mathrm{C}$
$\mathrm{T}_{\infty}=20^{\circ} \mathrm{C}$
$\mathrm{h}=200 \mathrm{~W} / \mathrm{m}^{2} \mathrm{~K}$
$\mathrm{c}=400 \mathrm{~J} / \mathrm{kgK}$
$\mathrm{k}=400 \mathrm{~W} / \mathrm{mK}$
$\rho=9000 \mathrm{~kg} / \mathrm{m}^{3}$
$\mathrm{T}=$ ?
$\mathrm{t}=90 \mathrm{sec}$
$\mathrm{L}_{\mathrm{c}}=\frac{\mathrm{V}}{\mathrm{A}_{\mathrm{s}}}=\frac{\frac{4}{3} \pi \mathrm{R}^{3}}{4 \pi \mathrm{R}^{2}}=\frac{\mathrm{R}}{3}=0.01$
Biot number $\mathrm{Bi}=\frac{\mathrm{hL}_{\mathrm{c}}}{\mathrm{k}}=\frac{200 \times 0.01}{400}$

$$
=5 \times 10^{-3}
$$

$\mathrm{Bi}<0.1$ hence lumped analysis is valid

$$
\frac{\mathrm{T}-\mathrm{T}_{\infty}}{\mathrm{T}_{0}-\mathrm{T}_{\infty}}=\mathrm{e}^{\frac{-\mathrm{ht}}{\frac{\mathrm{\rho LL}}{\mathrm{c}}}}
$$

$$
\mathrm{T}=\mathrm{T}_{\infty}+\left(\mathrm{T}_{0}-\mathrm{T}_{\infty}\right) \mathrm{e}^{\frac{-\mathrm{ht}}{\rho \mathrm{cL}_{\mathrm{c}}}}
$$

$$
\mathrm{T}=141^{\circ} \mathrm{C}
$$

55. Three masses are connected to a rotating shaft supported on bearings $A$ and $B$ as shown in the figure. The system is in a space where the gravitational effect is absent. Neglect the mass of shaft and rods connecting the masses. For $m_{1}=10 \mathrm{~kg}, \mathrm{~m}_{2}=5 \mathrm{~kg}$ and $\mathrm{m}_{3}=2.5 \mathrm{~kg}$ and for a shaft angular speed of $1000 \mathrm{radian} / \mathrm{s}$, the magnitude of the bearing reaction (in N ) at location B is $\qquad$


## 55. Ans: 0

Sol: $\mathrm{F}_{1}=\mathrm{m}_{1} \mathrm{r}_{1} \omega^{2}=10 \times 0.1 \times \omega^{2}=\omega^{2}$
$\mathrm{F}_{2}=\mathrm{m}_{2} \mathrm{r}_{2} \omega^{2}=5 \times 0.2 \times \omega^{2}=\omega^{2}$
$\mathrm{F}_{2}=\mathrm{m}_{2} \mathrm{r}_{2} \omega^{2}=2.5 \times 0.4 \omega^{2} \times \omega^{2}$
$\sum \mathrm{F}_{\mathrm{x}}=\omega^{2}\left[1+\cos 120^{\circ}+\cos 120^{\circ}\right]=0$
$\sum \mathrm{F}_{\mathrm{y}}=\mathrm{F}_{2} \cos 30^{\circ}-\mathrm{F}_{3} \cos 30^{\circ}=0$
$\therefore$ Net force $=0$
$\therefore$ Bearing reactions $=0 \mathrm{~N}$

Dingineering Academy Leading Institute for ESE/GATE/PSUs


## GENERAL APTITUDE

1. P looks at Q while Q looks at R . P is married, R is not. The number of pairs of people in which a married person is looking at an unmarried person is
(A) 0
(B) 1
(C) 2
(D) Cannot be determined
2. Ans: (B)

Sol: $\underset{\text { (married) }}{\mathrm{P}} \rightarrow \mathrm{Q} \rightarrow \underset{\text { (un married) }}{\mathrm{R}}$
P is a married person is looking Q
But Q is married (or) unmarried is not given so,
$\therefore$ Cannot be determined
02. If $a$ and $b$ are integers and $a-b$ is even, which of the following must always be even?
(A) $a b$
(B) $a^{2}+b^{2}+1$
(C) $a^{2}+b+1$
(D) $a b-b$
02. Ans: (D)

Sol: According to the given relation of $\mathrm{a}-\mathrm{b}=$ even, there is a possibility of odd-odd (or) even-even is equal to even
From the given option (D)
odd $\times$ odd - odd (or) even $\times$ even - even $\rightarrow$ is always even number
odd $=$ odd number, even $=$ even number
all other options are not satisfied this condition.
03. If you choose plan $P$, you will have to $\qquad$ plan Q , as these two are mutually $\qquad$ .
(A) forgo, exclusive
(B) forget, inclusive
(C) accept, exhaustive
(D) adopt, intrusive
03. Ans: (A)

Sol: Choosing plan ' P ', you will have for go plan ' Q '. Both are different plans so they are exclusive.
04. The ways in which this game can be played $\qquad$ potentially infinite.
(A) is
(B) is being
(C) are
(D) are being

## 04. Ans: (C)

Sol: Subject verb agreement 'Two ways' is plural so the verb also should be plural (are)
05. A couple has 2 children. The probability that both children are boys if the older one is a boy is
(A) $1 / 4$
(B) $1 / 3$
(C) $1 / 2$
(D) 1
05. Ans: (C)

Sol: Probability $=\frac{\text { no.of favorable cases }}{\text { total no.of possible cases }}$
Among two childrens (boys), the older one is a boy $=1$ and two childrens are boys only.
$\therefore$ Probability $=\frac{1}{2}$
06. "If you are looking for a history of India, or for an account of the rise and fall of the British Raj, or for the reason of the cleaving of the subcontinent into two mutually antagonistic parts and the effects this mutilation will have in the respective sections, and ultimately on Asia, you will not find it in these pages; for though I have spent a lifetime in the country, I lived too near the seat of events, and was too intimately associated with the actors, to get the perspective needed for the impartial recording of these matters."
Which of the following is closest in meaning to 'cleaving'?
(A) deteriorating (B) arguing
(C) departing
(D) splitting
06. Ans: (D)

Sol: Cleaving means to divide by or to separate into distinct parts.
07. There are 4 women $\mathrm{P}, \mathrm{Q}, \mathrm{R}, \mathrm{S}$, and 5 men $\mathrm{V}, \mathrm{W}, \mathrm{X}, \mathrm{Y}, \mathrm{Z}$ in a group. We are required to form pairs each consisting of one woman and one man. P is not to be paired with Z , and Y must necessarily be paired with someone. In how many ways can 4 such pairs be formed?
(A) 74
(B) 76
(C) 78
(D) 80

## 07. Ans: (B)

Sol: $\quad \mathrm{P}, \mathrm{Q}, \mathrm{R}, \mathrm{S} \rightarrow$ Women
V, W, X, Y, Z $\rightarrow$ Men
P is not to be paired with Z
Y must necessarily be paired with some one.
The possible ways $P$ can be paired with men $=4 \times 4($ without $z)=16$
The possible ways $Q$ can be paired with men $=4 \times 5=20$
The possible ways $S$ can be paired with men $=4 \times 5=20$
The total no. of ways $=16+20+20+20=76$
08. All people in a certain island are either 'Knights' or Knaves' and each person knows every other person's identify. Knights NEVER lie, and knaves ALWAYS lie.
P says "Both of us are knights". Q says "None of us are Knaves".
Which one of the following can be logically inferred from the above?
(A) Both P and Q are knights
(B) P is a knight; Q is a knave
(C) Both P and Q are knaves
(D) The identities of $\mathrm{P}, \mathrm{Q}$ cannot be determined
08. Ans: (D)
09. In the graph below, the concentration of a particular pollutant in a lake is plotted over (alternate) days of a month in winter (average temperature $10^{\circ} \mathrm{C}$ ) and a month in summer (average temperature $30^{\circ} \mathrm{C}$ ).


Consider the following statements based on the data shown above:
i. Over the given months, the difference between the maximum and the minimum pollutant concentrations is the same in both winter and summer.
ii. There are at least four days in the summer month such that the pollutant concentrations on those days are within 1 ppm of the pollutant concentrations on the corresponding days in the winter month.

Which one of the following options is correct?
(A) Only i
(B) Only ii
(C) Both i and ii
(D) Neither i nor ii

## 09. Ans: (B)

Sol: From the given graph ,
The difference between the maximum and the minimum pollutant concentrations in the winter $=8$
$-0=8 \mathrm{ppm}$
The difference between the maximum and the minimum pollutant concentrations in the summer $=$ $10.5-1.5=9 \mathrm{ppm}$
Over the given months, these differences are not equal.
$\therefore$ Therefore statement (i) is not correct.
From the given graph, the statement (ii) is correct.
10. $X$ bullocks and $Y$ tractors take 8 days to plough a field. If we halve the number of bullocks and double the number of tractors, it takes 5 days to plough the same field. How many days will it take X bullocks alone to plough the field?
(A) 30
(B) 35
(C) 40
(D) 45
10. Ans: (A)

Sol: No. of bullocks $=x$
No. of tractors $=y$,
From the given data,

$$
\begin{align*}
& (x+y)=8 \text { days, } 1 \text { day }(x+y)=\frac{1}{8}-\cdots--(i)  \tag{i}\\
& \left(\frac{x}{2}+2 y\right)=5 \text { days, } 1 \text { day }\left(\frac{x}{2}+2 y\right)=\frac{1}{5}
\end{align*}
$$

$x+y=\frac{1}{8}---(i) \times 2$
$2 x+2 y=\frac{1}{4}$
$\frac{x}{2}+2 y=\frac{1}{5}$

-     - 

$2 \mathrm{x}-\frac{\mathrm{x}}{2}=\frac{1}{20}$
$\frac{4 x-x}{2}=\frac{1}{20}$
$3 \mathrm{x}=\frac{1}{10}$
$\mathrm{x}=\frac{1}{30}^{\text {th }}$
One day work of x bullocks $=\frac{1}{30}$ th
$\therefore \mathrm{x}$ bullocks alone to plough the field $=30$ days

## USEFUL BOOKS FOR ESE(IES), GATE, PSUs

| GATE (Previous Questions \& Solutions) | IES (Previous Questions \& Solutions) |  |
| :---: | :---: | :---: |
| Electronics \& Communication Engineering | Electronics \& Telecommunication Engineering (Volume-I Obi) | Civil Engineering (Volume-I Obi) |
| Electrical Engineering | Electronics \& Telecommunication Engineering (Volume-II Obi) | Civil Engineering (Volume-ll Obi) |
| Mechanical Engineering | Electronics \& Telecommunication Engineering (Paper-I Conv) | Civil Engineering (Paper-I Conv) |
| Civil Engineering | Electronics \& Telecommunication Engineering (Paper-II Conv) | Civil Engineering (Paper-II Conv) |
| Computer Science \& Information Engineering | Electrical Engineering (Volume-I Obi) | Mechanical Engineering (Volume-I Obi) |
| Instrumentation Engineering | Electrical Engineering (Volume-II Obi) | Mechanical Engineering (Volume-II Obi) |
| General Aptitude (Numerical \& Verbal) | Electrical Engineering (Paper-I Conv) | Mechanical Engineering (Paper-I Conv) |
| GATE Practice Booklet (Vol-I),(Vol-II) | Electrical Engineering (Paper-II Conv) | Mechanical Engineering (Paper-II Conv) |
| Engineering Mathematics Solutions | General Studies \& Engineering Aptiude |  |
| Special Books For ISRO / PSUs (Previous Years Questions With Solutions \& Useful for BARC, SAlL, BEL, NPCIL, AAl \& OTHER PSUs) |  |  |

* GATE Solutions for more than $\mathbf{3 0}$ years
* IES Solutions for more than 32years
* Solutions, Chapterwise and Subjectwise

* You can Buy Online also


## TESTSERIES

| ES (Prelims \& Mains ) |  |  |  |
| :---: | :---: | :---: | :---: |
| Streams : EC, EE, ME, CE |  |  |  |
| Test Type | Prelims |  | Mains |
|  | Online | Offline | Offline |
| Chapter-wise Tests | 43 | - | - |
| Subject-wise Grand Tests | 31 | 20 | 08 |
| Revision Tests | - | - | 04 |
| Full Lenth Mock Tests | 08 | 04 | 04 |


|  |  |
| :--- | :---: |
| Streams : EC, EE, ME, CE, CS, IN, PI |  |
| Test Type | No. Of Tests (Online) |
| Chapter-wise Tests | 20 |
| Subject-wise Grand Tests | 40 |
| Full Lenth Mock Tests | 12 |

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