ACE
Engineering Academy

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ESE- 2018 (Prelims) - Offline Test Series-Test-15

ELECTRICAL ENGINEERING

SUBJECT: POWER SYSTEMS, POWER ELECTRONICS & DRIVES, AND SYSTEMS & SIGNAL PROCESSING

SOLUTIONS

01 Ans: (d)

Sol: $x(t) = \cos t + \sin\sqrt{3}t$

$$T_1 = \frac{2\pi}{1} = 2\pi$$

$$T_2 = \frac{2\pi}{\sqrt{3}} = \frac{2\pi}{\sqrt{3}}$$

$$\frac{T_1}{T_2} = \frac{2\pi}{\frac{2\pi}{\sqrt{3}}} = \sqrt{3} \Rightarrow \text{irrational number}$$

$\therefore x(t)$ is non-periodic

02. Ans: (c)

Sol: $y(t) = \sum_{k=-\infty}^{\infty} x(t)\,\delta(t - kT_s)$

$y(t)$ = ------ + $x(t)\ \delta(t+T_s)$ + $x(t)\ \delta(t)$ + $x(t)\ \delta(t-T_s)$ + -----

The above system is linear, time variant.

03. Ans: (b)

Sol: $\int_{-\infty}^{\infty} e^{-t}\ \delta'(t)dt = \frac{-d}{dt}\left[e^{-t}\right]_{t=0} = e^{-t}\Big|_{t=0} = 1$

04. Ans: (c)

Sol: $x(\infty) = \underset{Z\to 1}{\mathrm{Lt}}(z-1)X(z) = \underset{Z\to 1}{\mathrm{Lt}}\frac{z+1}{3(z+0.9)}$

$$= \frac{2}{3(1.9)} = 0.3508$$

05. Ans: (a)

Sol: $H(z) = \frac{z}{z+1}$

$$H_{inv}(z) = \frac{z+1}{z} = \frac{Y(z)}{X(z)} = 1 + z^{-1}$$

$Y(z) = X(z)+z^{-1}X(z)$

$y(n) = x(n)+x(n-1)$

06. Ans: (a)

Sol: From the given data the transfer function is

$$H(z)=\frac{k}{(z-2)\left(z-\frac{1}{2}\right)}$$

Non-anticipative means causal and it is possible only when ROC |z| > 2 ⇒ Right sided.

07. Ans: (d)

08. Ans: (c)

Sol: $x(n) = 1, \quad 0 \le n \le N-1$

$= 0, \text{ otherwise}$

$$X(k)=\sum_{n=0}^{N-1} x(n)e^{-j\frac{2\pi}{N}nk}=\sum_{n=0}^{N-1} e^{-j\frac{2\pi}{N}nk}=\frac{1-e^{-j2\pi k}}{1-e^{-j\frac{2\pi}{N}k}}$$

$X(0) = 0,\ k \neq 0$

$X(0) = N,\ k = 0$

$X(k) = N\delta(k)$

09. Ans: (c)

Sol: $y(n)-ay(n-1) = x(n)$

$$H(z)=\frac{Y(z)}{X(z)}=\frac{1}{1-az^{-1}}$$

$h(n) = (a)^n\, u(n)$

10. Ans: (d)

11. Ans: (c)

Sol: Using area property

$$\text{Area of}\left(e^{-\pi t^2}\right)\times \text{Area of}\left(e^{-\pi t^2}\right)=\text{Area of}\left(Ae^{-\frac{\pi t^2}{2}}\right)$$

$$\text{Area of}\left(e^{-at^2}\right)=\int_{-\infty}^{\infty} e^{-at^2}dt=\sqrt{\frac{\pi}{a}}$$

$$\sqrt{\frac{\pi}{\pi}}\times\sqrt{\frac{\pi}{\pi}}=A\sqrt{\frac{\pi}{\frac{\pi}{2}}}\Rightarrow A=\frac{1}{\sqrt{2}}$$

12. Ans: (a)

Sol: $r_{xh}(\tau)=x(\tau)*h(-\tau)=e^{-\tau}u(\tau)*e^{\tau}u(-\tau)$

Apply Fourier transform

$$S_{XH}(\omega)=\frac{1}{(1+j\omega)(1-j\omega)}=\frac{1}{2}\left[\frac{2}{\omega^2+1}\right]\xleftrightarrow{\text{I.F.T}}\frac{1}{2}e^{-|t|}$$

13. Ans: (b)

Sol: **Ex:** x(t) = u(t+1) u(1–t) = rect (t/2) is an energy signal but u(t+1) and u(1-t) are individually power signals. So statement (3) is FALSE.

14. Ans: (b)

Sol: The exponential Fourier series coefficient of x(t)

is $C_0=\frac{2}{\pi}$, $C_n=\frac{2}{\pi(1-4n^2)}$

Fundamental frequency is 250 Hz (not 125 Hz)

So the ideal filter will retain the d.c component in the output.

15. Ans: (c)

Sol: $tu(t-2)-2u(t)=(t-2+2)u(t-2)-2u(t)$

$$=-2u(t)+2u(t-2)+r(t-2)$$

16. Ans: (a)

Sol: $\text{Cos}^2(\omega_0 t)\ u(t) = \dfrac{1+\cos 2\omega_0 t}{2}u(t)$

$$=\frac{1}{2}u(t)+\frac{1}{2}\cos 2\omega_0 t\ u(t)$$

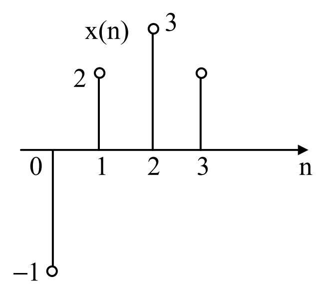
$$=\frac{1}{2s}+\frac{1}{2}\frac{s}{4\omega_0^2+s^2}$$

$$=\frac{1}{2}\left[\frac{4\omega_0^2+s^2+s^2}{s\left(4\omega_0^2+s^2\right)}\right]=\frac{1}{2}\times\frac{4\omega_0^2+2s^2}{s\left(4\omega_0^2+s^2\right)}$$

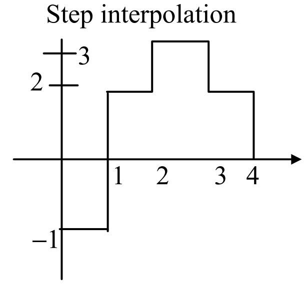
$$=\frac{2\omega_0^2+s^2}{s\left(4\omega_0^2+s^2\right)}$$

17. Ans: (b)

Sol:



Step interpolation



18. Ans: (b)

Sol: P: Delta function Fourier transform is constant function $\rightarrow$ 3.

Q: Gate function Fourier transform is sampling function $\rightarrow$ 4.

R: Gaussian function Fourier transform is Gaussian function $\rightarrow$ 2.

S: Sinusoidal function Fourier transform is Delta function $\rightarrow$ 3.

19. Ans: (c)

$\rightarrow$ The ON state voltage drop of SCR is 1- 1.5 V and for GTO 2-3 V

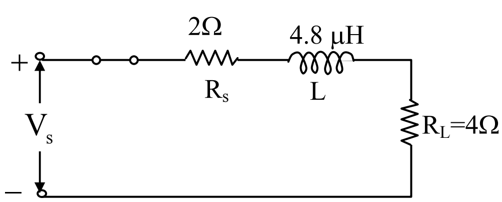
$\rightarrow$ GTO can be used for more switching frequency than that of SCR

$\rightarrow$ The GTO can be turned off by applying a negative gate-cathode voltage, therefore causing a sufficiently large negative gate current to flow.(i.e., large magnitude for small duration)

$\therefore$ So,options 1, 2 and 4 are true

20. Ans: (b)

Sol: At the instant of switch is closed



$$i = \frac{240}{6}\left[1 - e^{\frac{-6t}{4.8\times10^{-6}}}\right]$$

$$\frac{di}{dt} = \frac{240}{6}\left[e^{\frac{-6t}{4.8\times10^{-6}}}\right] \times \frac{6}{4.8\times10^{-6}}$$

$$\text{At } t = 0, \left(\frac{di}{dt}\right)_{max} = \frac{240}{4.8\times10^{-6}} = 50\text{A}/\mu\text{sec}$$

Voltage across SCR is given by V= R_s i

$$\left(\frac{dV}{dt}\right)_{max} = 2\times\left(\frac{di}{dt}\right)_{max}$$

$$= 100 \text{ V}/\mu\text{sec}$$

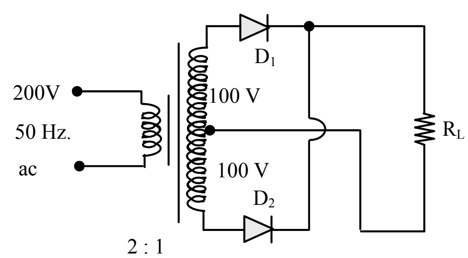
21. Ans: (a)

Power MOSFET is a low voltage, High current, power semiconductor device. It has positive temperature Coefficient gives the power MOSFET a good power handling capability as well as parallel operation is also possible. As the temperature of FET increases, The mobility of charge carriers decreases. so Thermal runaway is not possible in FET.

22. Ans: (a)

23. Ans: (d)

Sol:



As we know in centre tap full wave 1-ϕ rectifier circuit PIV of each diodes 2 V_m

$\therefore$ PIV = $2\sqrt{2} \times 100$ V

= 282.8 V

24. Ans: (a)

Sol: $\Rightarrow V_0 = \frac{2V_m}{\pi}\cos\alpha$

$$V_0 = \frac{2 \times 240\sqrt{2}}{\pi}\cos 60°$$

$= 108V$

$V_0 = I_0(R_L + 0.75) + E$

108=100+5(R+0.75)

R= 1.6 – 0.75

R = 0.85Ω

25. Ans: (a)

Sol: $I_0 = 60A$

$$I_{T_{avg}} = \frac{I_0 \times \frac{2\pi}{3}}{2\pi} = 20A$$

$$P_T = V_D \times I_{T_{avg}} = 20 \times 1.5$$

$$= 30W$$

26. Ans: (b)

Sol: Inversion Mode

$$I_0 = \frac{E - (-V_0)}{R} = \frac{E + V_0}{R}$$

$$10 \times 1.5 = 144 + \frac{2 \times 240\sqrt{2}}{\pi}\cos\alpha$$

$$\cos\alpha = \frac{-129.6}{216} = -0.6$$

$\alpha = 126.86°$

27. Ans: (c)

Sol: output ripple frequency = supply frequency × number of pulses in a cycle

= 50×6

= 300 Hz

28. Ans: (a)

Sol: Magnitude of reverse voltage across the scr,

$V_{ml} = 230\sqrt{2} = 325.26V$

Circuit turn of time, $\omega t_c = \pi - \alpha$ (when α > 60°)

$$\omega t_c = \frac{\pi}{2}$$

$$t_c = \frac{\frac{\pi}{2}}{2\pi \times 60} = 4.16 \text{ msec}$$

29. Ans: (c)

Sol: $K = \frac{2L}{RT} = \frac{2 \times 0.7 \times 10^{-3}}{1 \times 2000 \times 10^{-6}} = 0.7$

$K_{c_r} = (1 - D) = 0.7$

As k = K_{cr}

So,nature of current flowing through inductor is Boundary of continuous and discontinuous in nature.

30. Ans: (d)

31. Ans: (b)

32. Ans: (b)

Sol: $V_{01,rms} = \frac{4V_s}{\sqrt{2}\pi} = 108.04\,V$

$I_{01,rms} = \frac{250}{\sqrt{2}}, \cos\phi$

$= \cos 30° = 0.866$

$P_0 = V_{01,rms} I_{01,rms} . \cos\phi = 16.54\text{kW}$

33. Ans: (a)

Sol: turn - on loss

$= \left[\frac{VI}{6} \times t_{on}\right] f$

$= \frac{300 \times 200}{6} \times 1 \times 10^{-6} \times 10 \times 10^{3}$

$= 100\text{W}$

Conduction loss $= 2.1 \times 200 \times 0.5$

$= 210\text{W}$

34. Ans: (a)

Sol: $\frac{V_0}{V_{ml}} = \frac{\frac{3V_{ml}}{\pi}\cos\alpha}{V_{ml}}$

$\Rightarrow \frac{3}{\pi}\cos\alpha = 0.9549\cos\alpha$

35. Ans: (b)

Sol: Half bridge inverter power delivered to load

$$\Rightarrow P_1 = \frac{V_{or}^2}{R} = \frac{V_{dc}^2}{4R}$$

Full bridge inverter power delivered to load

$$\Rightarrow P_2 = \frac{V_{or}^2}{R}$$

$P_2 = 4P_1$

36. Ans: (c)

Sol: $$V_L = \frac{4V_s}{n\pi}.\cos\left(\frac{n\pi}{6}\right).\sin\left[n(\omega t + \frac{\pi}{6}\right]$$

$$100 = \frac{\frac{4V_s}{\pi}.\cos\left(\frac{\pi}{6}\right)}{\sqrt{2}}$$

$$100 = 0.9\,V_S \times \cos 30^\circ$$

$V_s = 128.3$ V

37. Ans: (d)

Sol: $$V_{\ell 5} = \frac{3V_s}{5\pi}.\sin\left[5\omega t + \frac{5\pi}{3}\right]$$

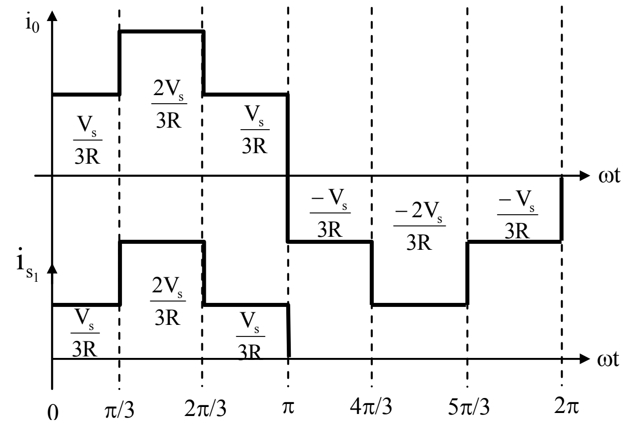
$$V_{\ell 5_{rms}} = \frac{\frac{3V_s}{5\pi}}{\sqrt{2}}$$

$$= 0.954 \times 10 \times \sqrt{2}$$

$V_{5,\,rms} = 13.5$ V

38. Ans: (a)

Sol:



$$(i_s)_{rms} = \sqrt{\left[\left(\frac{V_s}{3R}\right)^2 \times \frac{\pi/3}{2\pi} \times 2\right] + \left[\left(\frac{2V_s}{3R}\right)^2 \times \frac{\pi/3}{2\pi}\right]}$$

$$(i_s)_{rms} = \frac{V_s}{3R} = \frac{600}{3 \times 10} = 20\text{A}$$

39. Ans: (b)

Sol: In a AC voltage controller

$$\text{Power factor} = \frac{V_{or}}{V_S}$$

$$\text{Per unit power} = \frac{\text{actual power}}{\text{Rated power}}$$

$$= \frac{(V_{or})^2 / R}{V_S^2 / R}$$

$$\therefore \text{ Power factor } = \frac{V_{or}}{V_S} = \sqrt{\text{Per unit power}}$$

40. Ans: (a)

Sol: $$\frac{N}{2N}=\frac{2\frac{V_m}{\pi}\cos\alpha}{\frac{V_m}{\pi}[1+\cos\alpha]}\Rightarrow 1+\cos\alpha=4\cos\alpha$$

$\Rightarrow \cos\alpha = 1/3$

$\Rightarrow \alpha = 70.528^0$

41. Ans: (a)

Sol: Rated Shunt Compensation=VI $\tan\alpha$

$= 205 \times 105 \tan 45^o$

$= 21.6$ kVAR

Power factor, $\cos\alpha = \cos 45^0 = 0.707$

42. Ans: (a)

Sol: Given data,

Maximum demand = 50 MW,

Load factor = 80%, plant capacity factor = 50%

$$\because \text{Load factor} = \frac{\text{average load}}{\text{maximum demand}}$$

$\Rightarrow$ average load $= 0.8 \times 50$ MW

$= 40$ MW

$$\because \text{Plant capacity factor} = \frac{\text{average demand}}{\text{installed capacity}}$$

$$\Rightarrow \text{Installed capacity} = \frac{40}{0.5} = 80\text{ MW}$$

Then, reserve capacity of the plant

= installed capacity – maximum demand

= 80 – 50 = 30 MW

43. Ans: (c)

Sol: **Run of the river type:** It is a type of hydro electric plant where little or no water storage is provided.

Pondage type: It is a medium head hydro electric plant. It has small amount of water storage. They may be used in run of the river hydro electric plant in lean period.

Reservoir type: It is a high head plant consisting of a large dam.

44. Ans: (d)

Sol: Nuclear plants have a high capital cost in comparison to running cost, therefore, they are generally used as base load plant therefore statement-1 is wrong.

The rate of nuclear reaction can be lowered by small margin so that load on the nuclear power plant can be reduced by only a small margin below its fall load value. Tripping of lines may lead to shutting down of the plant itself.

Therefore statement-II is wrong.

45. Ans: (a)

Sol: Given data,

$$\frac{dC_1}{dP_1} = 0.2\ P_1 + 40$$

$$\frac{dC_2}{dP_2} = 0.4\ P_2 + 30$$

And $P_1 + P_2 = 220$ …………(1)

For optional economic operation,

$$\frac{dC_1}{dP_1} = \frac{dC_2}{dP_2}$$

$\Rightarrow 0.2\ P_1 + 40 = 0.4\ P_2 + 30$

$\Rightarrow P_1 - 2P_2 = -50$ …………(2)

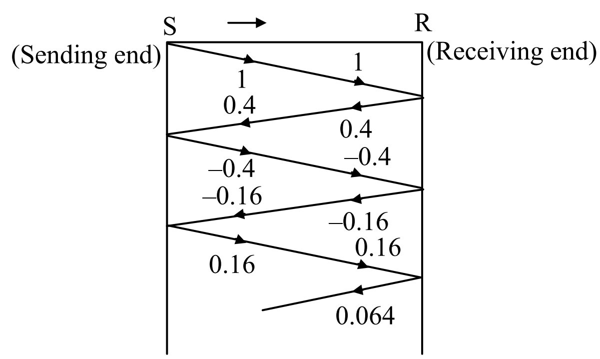
Now from equation (1) – equation (2)

$3P_2 = 270 \Rightarrow P_2 = 90$ MW

And $P_1 = 130$ MW

46. Ans: (d)

Sol: After infinite reflections, steady state is achieved (see the diagram)



fig(i)
(Bewley Lattice diagram)

Now, voltage at the receiving end would be,

$V_R(1+0.4) - (0.4+0.16) + (0.16+0.064)$……

$\Rightarrow V_R = (1+0.4)\ [1+(0.4)^2 + \ldots\ldots\{(0.4) + (0.4)^3 + \ldots..\}]$

$$\Rightarrow V_R = (1+0.4)\left[\frac{1}{1-(0.4)^2} - \frac{(0.4)}{1-(0.4)^2}\right]$$

$$\Rightarrow V_R = 1.4\left[\frac{1-0.4}{1-(0.4)^2}\right]$$

$$\Rightarrow V_R = 1.4\left[\frac{0.6}{(1+0.4)(1-0.4)}\right]$$

$$= 1.4\left[\frac{0.6}{1.4\times 0.6}\right]$$

$$= 1\text{V}$$

47. Ans: (c)

Sol: The nominal pH value of water is equal to 8.5, which is to be maintained in steam raising thermal power station.

48. Ans: (b)

49. Ans: (a)

Sol: Given data,

$v(t) = 100\cos\omega t$, $Z = 1.25\angle 60°\Omega$

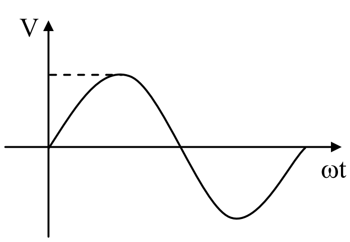
Then, $i(t) = \dfrac{100}{1.25}\cos(\omega t - 60°)$

$= 80\cos(\omega t - 60°)$

50. Ans: (a)

51. Ans: (c)

Sol: The design of overhead line insulator is based on peak voltage.



$V_m = \sqrt{2}\, V_{ph}$ (rms)

$= \sqrt{2}\dfrac{V}{\sqrt{3}}$

52. Ans: (b)

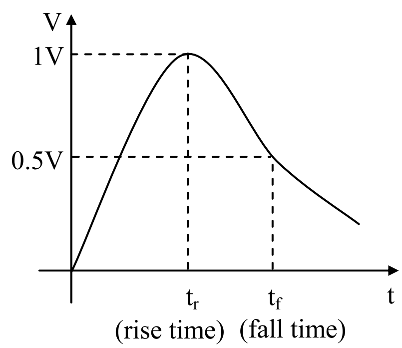
Sol: Standard representation of lightening impulse wave is

$V/t_r/t_f$

Where, V is the crest value of the voltage

t_r is the rise time

t_f is the fall time.



53. Ans: (a)

Sol: In sending end capacitor model no charging current component flows in the line impedance, so voltage drop is more and resultant sending end voltage is more for given receiving end voltage at lagging load condition.

54. Ans: (c)

Sol: P_{max} is more if 'X' of line is low

$X = 2\pi fL$, $\quad L = 2\times 10^{-7} ln\left(\dfrac{GMD}{GMR}\right)$

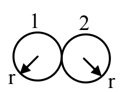
To get more P_{max}, GMD should be low and GMR should be high.

55. Ans: (c)

Sol: In lossless long line model No load power loss is $\frac{I_c^2 R}{3}$

56. Ans: (a)

Sol:



Self GMD = $\sqrt{r' \times 2r}$

$= \sqrt{0.7788r \times 2r}$

$= 1.248$ cm $\quad (\therefore r = 1\text{cm})$

57. Ans: (b)

Sol: $A = D = \cos\beta l$, $B = jZ_c \sin\beta l$, $C = j\frac{1}{Z_C}\sin\beta l$

As frequency increases, $\beta = \omega\sqrt{LC} \Rightarrow \beta\uparrow$

So $|A|\downarrow |B|\uparrow |C|\uparrow |D|\downarrow$

58. Ans: (c)

Sol: $X_{p.u\,(LV)} = 0.121 \times \frac{400}{(22)^2}$

$= 0.1$

$X_{p.u(HV)} = X_{p.u\,(LV)}$

$= 0.1$

$$X_{p.u\,(HV)New} = X_{p.u\,HV\,old}\frac{MVA_{new}}{MVA_{old}}\left(\frac{kV_{old}}{kV_{new}}\right)^2$$

$$= 0.1 \times \frac{100}{400} \times \left(\frac{220}{230}\right)^2$$

$= 0.0228$

59. Ans: (c)

Sol: For LLG fault, $I_{positive} = I_{negative} + I_{zero}$

Hence given data satisfies the above condition.

60. Ans: (a)

Sol: String efficiency in suspension type insulator can be improved by the following methods:

1. using a longer cross arm
2. using a guard ring
3. using graded insulator discs

61. Ans: (b)

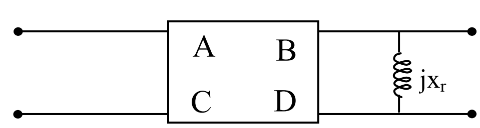
Sol: $M = \frac{SH}{\pi f} = \frac{100 \times 8}{3.14 \times 50}$

$= 5.09$ MJ-sec/Elec rad

$M = \frac{5.09}{2} = 2.54$ MJ-sec/ Mech rad.

62. Ans: (c)

Sol:



$$\begin{bmatrix} A_{eq} & B_{eq} \\ C_{eq} & D_{eq} \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 1/jx_r & 1 \end{bmatrix}$$

$\Rightarrow A_{eq} = |A| + \dfrac{|B|}{x_r}$ as $A_{eq} = 1$

$\Rightarrow |A| + \dfrac{|B|}{x_r} = 1 \Rightarrow x_r = \dfrac{|B|}{1-|A|}$

For $\Delta \Rightarrow x_r(\Delta) = 3 \times \dfrac{|B|}{1-|A|}$

63. Ans: (c)

Sol: $\dfrac{dp}{d\delta} = 3\cos\delta$, $\left.\dfrac{dp}{d\delta}\right|_{\delta=60^o} = 3\times\cos 60^o = 1.5$ p.u

64. Ans: (b)

Sol: $V_{a0} = -I_{a0}(Z_0 + 3Z_n)$

$Z_0 + 3Z_n = \dfrac{V_{a0}}{-I_{a0}} = \dfrac{-0.3}{+j2} = j0.15$

$Z_n = 0.033$p.u

65. Ans: (b)

Sol: ARV = $K_1\, K_2\, K_3.\, V_{max} \sin\phi$

$= 0.9 \times 1 \times 1 \times \dfrac{66}{\sqrt{3}} \times \sqrt{2} \times \sqrt{1-(0.25)^2}$

= 46.96 kV

66. Ans: (a)

67. Ans: (b)

Sol: If the fault is away from the relay, then the impedance seen by the relay is more.

68. Ans: (a)

69. Ans: (a)

70. Ans: (a)

71. Ans: (a)

Sol: Secondary cells are rechargeable in comparison to primary cells that are not rechargeable.

Hence, life of secondary cell is more than a primary cell.

The main reason for the rechargeable property of secondary cells is the reversible redone reaction given power input also the component are least degraded during such reversible reaction.

72. Ans: (a)

Sol: For discontinuous mode of operation the ripple content will be high and Average value of output voltage is more as compared with continuous mode output average value.

73. Ans: (b)

74. Ans: (a)

Sol: $H(S)_{APF} = \dfrac{s-\alpha}{s+\alpha}$

75. Ans: (d)

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6 EE DUSHYANT SINGH
8 EE APOORVA GUPTA
9 EE KIRAN BABU KONERU
7
IN TOP 10 RANKS
and many more...
ME
3 ME SAURABH
4 ME AMIT KUMAR RAI
6 ME ANKAN GUPTA
7 ME DHRUW JHA
9 ME ACHARAJ GUPTA
5
IN TOP 10 RANKS
27
Ranks in Top 10 in ESE-2017
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