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# GATE-2020

Questions with Detailed Solutions

## ***ELECTRONICS & COMMUNICATION ENGINEERING***

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**GATE - 2020**  
**Electronics & Communication Engg.**  
**Question with Detailed Solutions**

**02/02/20**

**SUBJECTWISE WEIGHTAGE**

S. No.	NAME OF THE SUBJECT	1 MARK QUESTIONS	2 MARKS QUESTIONS	Total Marks
1	Verbal Ability	2	3	8
2	Numerical Ability	3	2	7
3	Engineering Mathematics	5	3	11
4	Network Theory	3	2	7
5	Control Systems	2	3	8
6	Digital Circuits & Microprocessors	3	3	9
7	Signals & System	2	3	8
8	EDC & VLSI	2	4	10
9	Analog Circuits	3	5	13
10	EMT	3	4	11
11	Communication Systems	2	3	8
<b>Total No. of Marks</b>		<b>30</b>	<b>35</b>	<b>100</b>

**Section : General Aptitude**

01. A superadditive function  $f(\cdot)$  satisfies the following property

$$f(x_1 + x_2) \geq f(x_1) + f(x_2)$$

Which of the following functions is a superadditive function for  $x > 1$  ?

- (a)  $\frac{1}{x}$
- (b)  $e^x$
- (c)  $e^{-x}$
- (d)  $\sqrt{x}$

**01. Ans: (b)**

**Sol:**  $a^m$  is super additive function, if  $a > 1$ .

example  $2^5 > 2^2 + 2^3$

$$f(x_1 + x_2) > f(x_1) + f(x_2)$$

So,  $e^x$  is super additive function. ( $\because e > 1$ )

02. The Canadian constitution requires equal importance be given to English and French. Last year, Air Canada lost a lawsuit, and had to pay a six-figure fine to French-speaking couple after they filed a complaints about formal in-flight announcements in English lasting 15 seconds, as compared to informal 5 seconds messages in French.

The French-speaking couple were upset at \_\_\_\_\_.

- (a) the in-flight announcement being made in English.
- (b) the English announcements being clearer than French ones
- (c) equal importance being given to English and French.
- (d) the English announcements being longer than French ones.

**02. Ans: (d)**

03. The global financial crisis in 2008 as considered to be the most serious world-wide financial crisis, which started with the sub-prime landing crisis in USA in 2007. The sub-prime landing crisis led to the banking crisis in 2008 with the collapse of Lehman Brothers in 2008. The sub-prime landing refers to the provision of loans to those borrowers

who may have difficulties in repaying loans, and its arises because of excess liquidity following the East Asian crisis.

Which one of the following sequences show the correct precedence as per the given passage?

- (a) Banking crisis — Sub-prime lending crisis — Global financial crisis — East Asian crisis
- (b) East Asian crisis — Sub-prime landing crisis — Banking crisis — Global financial crisis
- (c) Sub-prime lending crisis — Global financial crisis — Banking crisis — East Asian crisis
- (d) Global financial crisis — East Asian crisis — Banking crisis — Sub-prime landing crisis

**03. Ans: (b)**

04. a,b,c are real numbers. The quadratic equation  $ax^2 - bx + c = 0$  has equal roots, which is  $\beta$ , then

- (a)  $\beta^2 = ac$
- (b)  $\beta = b/a$
- (c)  $b^2 \neq 4ac$
- (d)  $\beta^3 = bc / (2a^2)$

**04. Ans: (d)**

**Sol:**  $ax^2 - bx + c = 0$

$$\text{Sum of roots} = \beta + \beta = \frac{b}{a} \Rightarrow 2\beta = \frac{b}{a} \text{ ----- (1)}$$

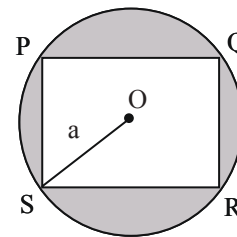
$$\text{Product of roots} = \beta * \beta = \frac{c}{a} \Rightarrow \beta^2 = \frac{c}{a} \text{ ----- (2)}$$

$$\text{Now (1) } \times \text{ (2)} \Rightarrow (2\beta)(\beta^2) = (b/a)(c/a)$$

$$(2\beta^3) = bc/a^2$$

$$\beta^3 = bc/(2a^2)$$

05. A circle with centre O is shown in the figure. A rectangle PQRS of maximum possible area is inscribed in the circle. If the radius of the circle is a, then the area of the shaded portion is \_\_\_\_\_.



Find shaded area

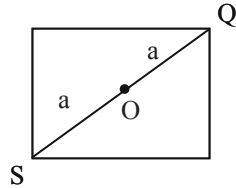
- (a)  $\pi a^2 - 3a^2$
- (b)  $\pi a^2 - 2a^2$
- (c)  $\pi a^2 - a^2$
- (d)  $\pi a^2 - \sqrt{2} a^2$

**05. Ans: (b)**

**Sol:** Area of shaded portion

$$= \text{Area of circle} - \text{Area of rectangle}$$

Area of rectangle is maximum, when it becomes square.



$$\text{Diagonal} = 2a$$

$$\text{Area of square} = \frac{1}{2}(\text{diagonal})^2 = 2a^2$$

$\therefore$  Area of shaded portion

$$= \text{Area of circle} - \text{Area of square}$$

$$= \pi a^2 - 2a^2$$

06. Select the word that fits the analogy:

Explicit: Implicit:: Express: \_\_\_\_\_

- (a) Repress (b) Impress  
(c) Suppress (d) compress

**06. Ans: (c)**

07. The untimely loss of life is a cause of serious global concern as thousands of people get killed \_\_\_\_\_ accidents every year while many other die \_\_\_\_\_ diseases like cardio vascular disease, cancer, etc.

- (a) from, of  
(b) from, from  
(c) during, from  
(d) in, of

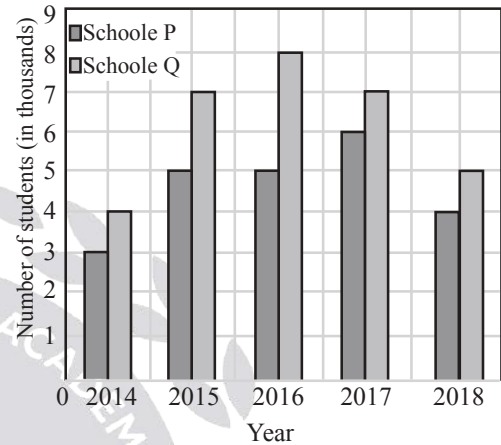
**07. Ans: (d)**

08. He was not only accused of theft \_\_\_\_\_ of conspiracy.

- (a) rather than  
(b) rather  
(c) but also  
(d) but even

**08. Ans: (c)**

09. The following figure shows the data of students enrolled in 5 years (2014 to 2018) for two schools P and Q. During this period, the ratio of the average number of the students enrolled in school P to the average of the difference of the number of students enrolled in schools P and Q is \_\_\_\_\_



- (a) 8 : 23 (b) 31 : 23  
(c) 23 : 8 (d) 23 : 31

**09. Ans: (c)**

**Sol:** Average number of students enrolled in school P in 5 years =  $\frac{3000 + 5000 + 5000 + 6000 + 4000}{5} = 4600$

Average number of students enrolled in school Q in 5 years =  $\frac{4000 + 7000 + 8000 + 7000 + 5000}{5} = 6200$

Average of the difference of the number of students in school P and Q =  $6200 - 4600 = 1600$

Desired ratio =  $\frac{4600}{1600} = \frac{23}{8}$   
23 : 8

10. It is quarter past three in your watch. The angle between the hour hand and the minute hand is \_\_\_\_\_

- (a) 0° (b) 7.5°  
(c) 22.5° (d) 15°

**10. Ans: (b)**

**Sol:** Time: 03 : 15

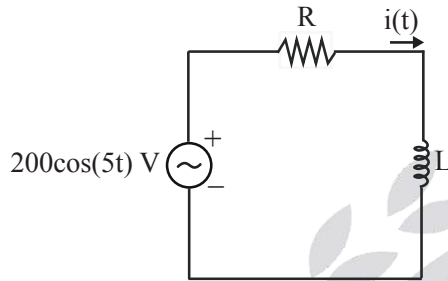
$$\text{Angle between hands } \theta = \left| 30h - \frac{11m}{2} \right|$$

Here, h = 3 and m = 15

$$\text{So, } \theta = \left| 30 \times 3 - \frac{165}{2} \right| = 7.5^\circ$$

**Section : Electronics & Communication Engineering**

01. The current in the RL-circuit shown below is  $i(t) = 10 \cos(5t - \pi/4)A$ .  
The value of the inductor (**rounded off to two decimal places**) is \_\_\_\_ H.



**01. Ans: 2.828**

**Sol:**  $\bar{V} = 200 \angle 0^\circ$

$\bar{I} = 10 \angle -45^\circ$

$Z = \frac{V}{I} = 20 \angle +45^\circ$

$Z = 14.14 + j14.14$



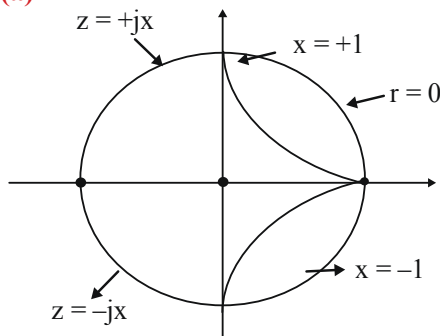
$X_L = \omega L = 14.14 \Rightarrow L = \frac{14.14}{\omega} = \frac{14.14}{5}$

$L = 2.828H$

02. The impedances  $Z = jX$ , for all  $X$  in the range  $(-\infty, \infty)$ , map to the Smith chart as
- a circle of radius 1 with centre at  $(0, 0)$
  - a point at the centre of the chart.
  - a circle of radius 0.5 with centre at  $(0.5, 0)$
  - a line passing through the centre of the chart.

**02. Ans: (a)**

**Sol:**



Circle of radius 1 with centre at  $(0, 0)$  indicates pure inductance and capacitive load.

03. For a vector field  $\vec{A}$ , which one of the following is FALSE ?
- $\vec{A}$  is irrotational if  $\nabla^2 \vec{A} = 0$
  - $\nabla \times (\nabla \times \vec{A}) = \nabla(\nabla \cdot \vec{A}) - \nabla^2 \vec{A}$
  - $\nabla \times \vec{A}$  is also another vector field
  - $\vec{A}$  is solenoidal if  $\nabla \cdot \vec{A} = 0$

**03. Ans: (a)**

**Sol:** For a vector field  $\vec{A}$

- $\vec{A}$  is irrotational (or) conservative only if  $\nabla \times \vec{A} = 0$
- $\nabla \times (\nabla \times \vec{A}) = \nabla(\nabla \cdot \vec{A}) - \nabla^2 \vec{A}$  is used to obtain EM wave equation.
- curl of a vector,  $\vec{A}$  is an another vector field i.e.  $\nabla \times \vec{A}$  is another vector field.
- $\vec{A}$  is said to be solenoidal if  $\nabla \cdot \vec{A} = 0$  Therefore option (a) is FALSE

04. A 10-bit D/A converter is calibrated over the full range from 0 to 10V. If the input to the D/A converter is 13A (in hex), the output (**rounded off to three decimal places**) is \_\_\_\_ V.

**04. Ans: 3.066**

**Sol:** DAC output = Number of steps for given digital input  $\times$  step size

Where Number of steps for digital input  $13A_{16}$  is

$\Rightarrow 1 \times 16^2 + 3 \times 16^1 + 10 \times 16^0 = 314$

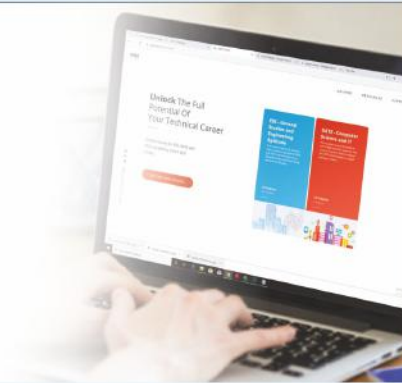
step size =  $\frac{10}{2^{10}} = \frac{10}{1024}$

Thus, DAC output

$= 314 \times \frac{10}{1024} = \frac{3140}{1024} = 3.066$  volts.

05. The general solution of  $\frac{d^2y}{dx^2} - 6\frac{dy}{dx} + 9y = 0$  is
- $y = C_1 e^{3x} + C_2 e^{-3x}$
  - $y = (C_1 + C_2 x) e^{-3x}$
  - $y = C_1 e^{3x}$
  - $y = (C_1 + C_2 x) e^{3x}$

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**05 Ans: (d)**

**Sol:** Given  $f(D)y = 0$ , where  $f(D) = D^2 - 6D + 9$

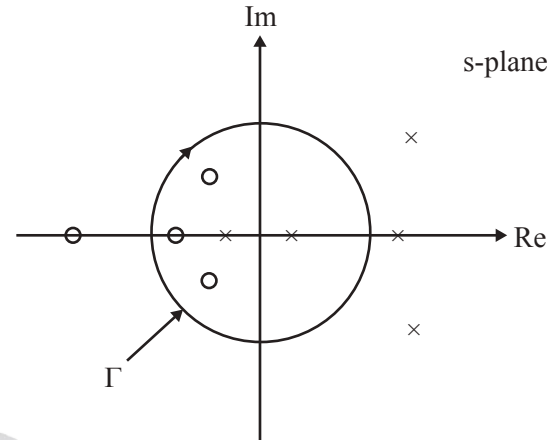
$\Rightarrow$  Auxiliary equation is  $f(m) = 0$

$\Rightarrow m^2 - 6m + 9 = 0$

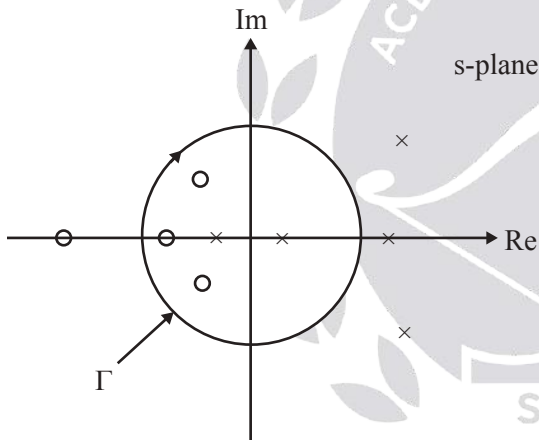
$\Rightarrow m = 3, 3$  are real and equal roots

$\therefore$  The general solution of given v differential equation is  $y = (C_1 + C_2x)e^{3x}$ .

$\therefore$  option (d) is correct.



06. The pole-zero map of a rational function  $G(s)$  is shown below. When the closed contour  $\Gamma$  is mapped into the  $G(s)$ -plane, then the mapping encircles.

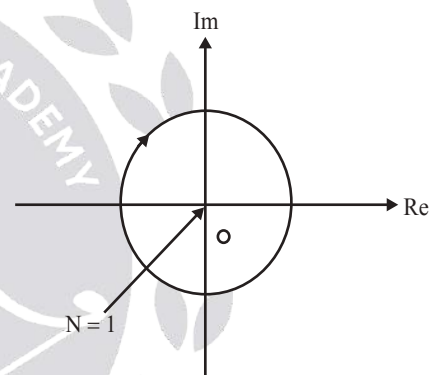


- (a) the origin of the  $G(s)$ -plane once in the counter-clockwise direction.
- (b) the point  $-1+j0$  of the  $G(s)$ -plane once in the counter-clockwise direction.
- (c) the origin of the  $G(s)$ -plane once in the clockwise direction.
- (d) the point  $-1+j0$  of the  $G(s)$ -plane once in the clockwise direction.

**06. Ans: (c)**

**Sol:** Once encircles the origin in the clock wise direction.

$G(s)$  - plane



07. The output  $y[n]$  of a discrete-time system for an input  $x[n]$  is

$$y[n] = \max_{-\infty \leq k \leq n} |x[k]|$$

The unit impulse response of the system is

- (a) unit step signal  $u[n]$
- (b) 1 for all  $n$
- (c) 0 for all  $n$
- (d) unit impulse signal  $\delta[n]$

**07. Ans: (a)**

**Sol:**  $y(n) = \max |x(k)| \quad -\infty \leq k \leq n$

The unit impulse response is

If we apply  $x(n) = \delta(n)$

$$y(n) = \max |\delta(k)| = 1 \quad n \geq 0$$

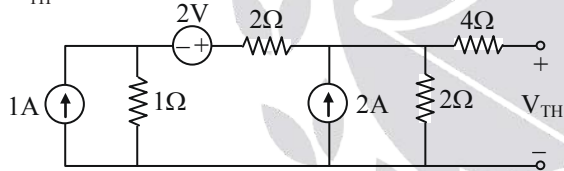
$$= u(n)$$

08. Consider the recombination process via bulk traps in a forward biased pn homojunction diode. The maximum recombination rate is  $U_{max}$ . If the electron and the hole capture cross-sections are equal, which one of the following is FALSE ?
- (a)  $U_{max}$  depends exponentially on the applied bias
  - (b)  $U_{max}$  occurs at the edges of the depletion region in the device
  - (c) With all other parameters unchanged,  $U_{max}$  decreases if the intrinsic carrier density is reduced.
  - (d) With all other parameters unchanged,  $U_{max}$  increases if the thermal velocity of the carrier increases.

**08. Ans: (c)**

**Sol:** Intrinsic carrier density will not affect generation and recombination rate. so, statement (c) is false.

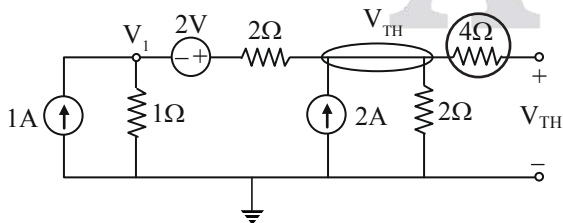
09. In the circuit shown below, the Thevenin voltage  $V_{TH}$  is



- (a) 2.8 V
- (b) 4.5 V
- (c) 3.6 V
- (d) 2.4 V

**09. Ans: (c)**

**Sol: Nodal Analysis:**



$$-1 + \frac{V_1}{1} + \frac{(V_1 - V_{TH} + 2)}{2} = 0$$

$$3V_1 - V_{TH} = 0 \quad (1)$$

$$\frac{V_{TH}}{2} - 2 + \frac{(V_{TH} - V_1 - 2)}{2} = 0$$

$$-V_1 + 2V_{TH} = 6 \quad (2)$$

By multiply equation (2) with 3, then we get

$$-3V_1 + 6V_{TH} = 18 \quad (2A)$$

By adding equation (1) with (2A), then we get

$$5V_{TH} = 18$$

$$V_{TH} = \frac{18}{5} = 3.6V$$

10. The two sides of a fair coin are labelled as 0 and 1. The coin is tossed two times independently. Let M and N denote the labels corresponding to the outcomes of those tosses. For a random variable X, defined as  $X = \min(M, N)$ , the expected value  $E(X)$  (rounded off to two decimal places) is \_\_\_\_\_

**10. Ans: 0.25**

**Sol:** Coin tossed two times:

Outcomes  $X = \min(m, N)$

0 0 0

0 1 0

1 0 0

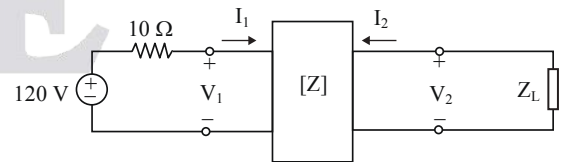
1 1 1

$$P(X = 0) = 3/4, \quad P(X = 1) = 1/4$$

$$E(X) = \sum_i x_i P(X = x_i)$$

$$E(X) = 0 \times \frac{3}{4} + 1 \times \frac{1}{4} = 0.25$$

11. In the given circuit, the two-port network has the impedance matrix  $[Z] = \begin{bmatrix} 40 & 60 \\ 60 & 120 \end{bmatrix}$ . The value of  $Z_L$  for which maximum power is transferred to the load is \_\_\_\_\_  $\Omega$ .

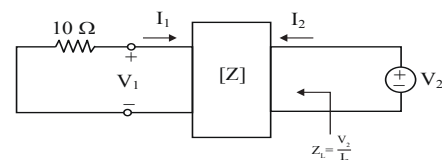


**11. Ans: 48**

**Sol:**  $V_1 = 40I_1 + 60I_2$  \_\_\_\_\_ (1)

$V_2 = 60I_1 + 120I_2$  \_\_\_\_\_ (2)

S-I  $Z_L = \frac{V_2}{I_2}$





also,

$$10 I_1 + V_1 = 0 \text{ _____ (3)}$$

(3) in (1)

$$-10I_1 = 40 I_1 + 60I_2$$

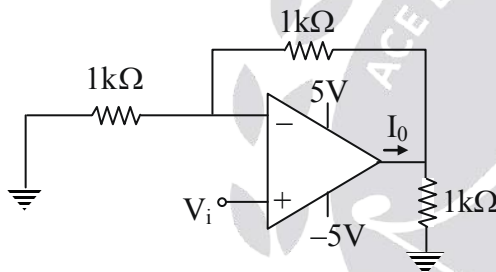
$$-50I_1 = 60 I_2 \rightarrow I_1 = -\frac{6}{5}I_2 \text{ _____ (4)}$$

$$(4) \text{ in (2) } V_2 = 60 \left[ \frac{-6}{5} \right] I_2 + 120I_2$$

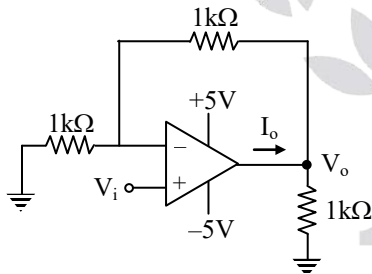
$$V_2 = -72 I_2 + 120I_2$$

$$V_2 = 48I_2 \Rightarrow Z_L = \frac{V_2}{I_2} = 48\Omega$$

12. In the circuit shown below, all the components are ideal. If  $V_i$  is +2V, the current  $I_0$  sourced by the op-amp is \_\_\_\_\_ mA.



**12. Ans: 6**  
**Sol:**



Given op-amp is in non-inverting mode, then output

$$V_o = \left(1 + \frac{R_f}{R_i}\right) V_{in} = \left(1 + \frac{1k}{1k}\right) + 2V = 4V$$

KCL at node  $V_o$

$$\frac{V_o - V_i}{1k} + \frac{V_o}{1k} - I_o = 0$$

$$I_o = \frac{4-2}{1k} + \frac{4}{1k}$$

$$I_o = 6\text{mA}$$

13. A transmission line of length  $3\lambda/4$  and having a characteristic impedance of  $50\Omega$  is terminated with a load of  $400\Omega$ . The impedance (rounded off to two decimal places) seen at the input end of the transmission line is \_\_\_\_\_  $\Omega$

**13. Ans: 6.25**

**Sol:** Given: Length of transmission line:  $l = \frac{3\lambda}{4}$   
 $Z_o = 50\Omega$   
 $Z_R = 400\Omega$

As length of the transmission line is  $\frac{3\lambda}{4}$ , (odd multiples of quarter wavelengths like  $\frac{\lambda}{4}, \frac{3\lambda}{4}, \frac{5\lambda}{4}$  ....) and hence this line must be a quarter wave transmission line.

Assume this quarter wave transmission line is

$$\begin{aligned} \text{lossless then } Z_{in} &= \frac{Z_o^2}{Z_R} \\ &= \frac{50^2}{400} \\ &= 6.25\Omega \end{aligned}$$

14. The random variable

$$Y = \int_{-\infty}^{\infty} W(t)\phi(t)dt,$$

$$\text{where } \phi(t) = \begin{cases} 1; & 5 \leq t \leq 7 \\ 0; & \text{otherwise} \end{cases}$$

and  $W(t)$  is a real white Gaussian noise process with two-sided power spectral density  $S_w(f) = 3$  W/Hz, for all  $f$ . The variance of  $Y$  is \_\_\_\_\_

**14. Ans: 6**

**Sol:**  $Y = \int_{-\infty}^{\infty} W(t)\phi(t)dt$   
Let  $\phi(t) = h(-(t-\tau)) \Rightarrow$  where  $\tau$  is the symbol duration

$$Y = \int_{-\infty}^{\infty} W(t)h(-(t-\tau))dt \text{ Let } t = \tau \Rightarrow dt = d\tau$$

$$Y = \int_{-\infty}^{\infty} W(\tau)h(\tau-t)d\tau$$

$$Y(t) = W(t) * h(t)$$

$$\Rightarrow S_Y(f) = |H(f)|^2 S_w(f)$$

$$\sigma_Y^2 = E[Y^2] - E[Y]^2$$

$$E[Y^2] = \int_{-\infty}^{\infty} S_Y(f)df = \int_{-\infty}^{\infty} |H(f)|^2 S_w(f)df$$

$$E[Y] = E\left[\int_{-\infty}^{\infty} W(t)\phi(t)dt\right]$$

$$\begin{aligned}
 &= E \left[ \int_{-\infty}^{\infty} E[W(t)]\phi(t) dt \right] \\
 &= 0 \\
 S_w(f) &= \frac{N_0}{2} \\
 &= \frac{N_0}{2} \int_{-\infty}^{\infty} |H(f)|^2 df \\
 &= \frac{N_0}{2} \int_{-\infty}^{\infty} |\phi(f)|^2 df (\because \phi(t) = h(-(t-\tau))) \\
 |\phi(f)|^2 &= |H(f)|^2 \\
 &= \frac{N_0}{2} \int_{-\infty}^{\infty} |\phi(t)|^2 dt (\text{from the rayleigh's energy theorem}) \\
 &= \left(\frac{N_0}{2}\right) E_\phi \\
 &= 3 \times 2 (\because E_\phi = 2) \\
 &= 6
 \end{aligned}$$

15. If  $v_1, v_2, \dots, v_6$  are six vectors in  $R^4$ , which one of the following statements is FALSE ?
- (a) These vectors are not linearly independent
  - (b) Any four of these vectors form a basis for  $R^4$
  - (c) It is not necessary that these vectors span  $R^4$
  - (d) If  $\{v_1, v_3, v_5, v_6\}$  spans  $R^4$ , then it forms a basis for  $R^4$

**15. Ans: (d)**

**Sol:** option (d) is a wrong statement.

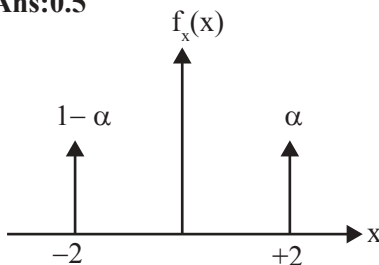
if  $\{v_1, v_3, v_5, v_6\}$  spans  $R^4$  then it may (or) may not be a basis for  $R^4$ .

i.e. To form a basis, the set  $\{v_1, v_3, v_5, v_6\}$  should be linearly independent set.

16. A binary random variable X takes the value +2 or -2. The probability  $P(X = +2) = \alpha$ . The value of  $\alpha$  (rounded off to one decimal place), for which the entropy of X is maximum, is \_\_\_\_\_

**16. Ans:0.5**

**Sol:**



Entropy will be maximum when the probabilities are equal i.e  $P(X = +2) = 1/2 = 0.5$

17. A single crystal intrinsic semiconductor is at a temperature of 300K with effective density of states for holes twice that of electrons. The thermal voltage is 26mV. The intrinsic Fermi level is shifted from mid-bandgap energy level by
- (a) 13.45 meV
  - (b) 18.02 meV
  - (c) 26.90 meV
  - (d) 9.01 meV

**17. Ans: (d)**

**Sol:**  $T = 300K, N_v = 2 N_c, V_T = 26mV$

$$E_F = \frac{E_c + E_v}{2} - \frac{KT}{2} \ln\left(\frac{N_c}{N_v}\right)$$

if  $N_c = N_v$  then  $E_{Fi} = \frac{E_c + E_v}{2} \Rightarrow$  Midband gap energy

Given  $N_v = 2N_c$

$$E_F = E_{Fi} - \frac{KT}{2} \ln\left(\frac{N_c}{2N_c}\right)$$

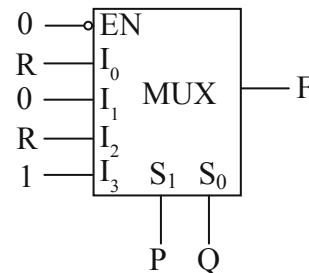
$$= E_{Fi} - \frac{KT}{2} \ln\left(\frac{1}{2}\right)$$

$$= E_{Fi} - \frac{0.026}{2} \ln\left(\frac{1}{2}\right)$$

$$= E_{Fi} + 9.01 \times 10^{-3}$$

$$= 9.01meV$$

18. The figure below shows a multiplexer where  $S_1$  and  $S_0$  are the select lines,  $I_0$  to  $I_3$  are the input data lines, EN is the enable line, and  $F(P, Q, R)$  is the output F is



- (a)  $PQ + \bar{Q}R$
- (b)  $P\bar{Q}R + \bar{P}Q$
- (c)  $P + Q\bar{R}$
- (d)  $\bar{Q} + PR$



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EEE		ECE / IN		CS & IT		CE		ME / PI	
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Networks	5 Q	Networks	6 Q	DS, PL & Algorithm	10 Q	SOM	5 Q	SOM	6 Q
Control System	5 Q	Control System	6 Q	DBMS	5 Q	FM & HM	5 Q	FM & HM	5 Q
Analog Electronics	4 Q	Analog Electronics	5 Q	Computer Networks	5 Q	Geo Technical Engg.	7 Q	TOM	6 Q
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Electrical Machines	8 Q	Signal & Systems	5 Q	Computer Organization	4 Q	Transportation	4 Q	Thermal	7 Q
Power System	7 Q	EDC & VLSI	5 Q	Theory of Computation	6 Q	RCC & STEEL	6 Q	Heat Mass Transfer	4 Q
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Numerical / Verbal Ability	5 Q	Numerical / Verbal Ability	5 Q	Numerical / Verbal Ability	5 Q	Numerical / Verbal Ability	5 Q	Numerical / Verbal Ability	5 Q

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**18. Ans: (a)**

**Sol:** As  $EN = 0 \rightarrow$  The multiplexer is Enabled.

$$\begin{aligned} \text{The output } F &= \bar{S}_1 \bar{S}_0 I_0 + \bar{S}_1 S_0 I_1 + S_1 \bar{S}_0 I_2 + S_1 S_0 I_3 \\ F &= \bar{P} \bar{Q} . R + \bar{P} . Q . 0 + P . \bar{Q} . R + P . Q . 1 \\ &= \bar{Q} R + P Q . \end{aligned}$$

19. The loop transfer function of a negative feedback system is

$$G(s)H(s) = \frac{K(s+11)}{s(s+2)(s+8)}.$$

The value of K, for which the system is marginally stable, is \_\_\_\_\_.

**19. Ans:160**

**Sol:** 
$$G(s)H(s) = \frac{K(s+11)}{s(s+2)(s+8)}$$

Characteristic equation:  $1 + G(s)H(s) = 0$

$$\begin{aligned} &: s(s+2)(s+8) + K(s+11) = 0 \\ &: s^3 + 10s^2 + 16s + Ks + 11K = 0 \\ &: s^3 + 10s^2 + (16+K)s + 11K = 0 \end{aligned}$$

$s^3$	1	$16+K$
$s^2$	10	$11K$
$s^1$	$\frac{10(16+K) - 11K}{10}$	
$s^0$	$11K$	

For marginal stability,

$$\left( \frac{10(K+16) - 11K}{10} \right) = 0$$

$$10K + 160 - 11K = 0$$

$$K = 160$$

20. The partial derivative of the function

$$f(x,y,z) = e^{1-x\cos y} + xze^{-\frac{1}{1+y^2}}$$

with respect to x at the point (1, 0, e) is

Options

- (a) 1      (b) 0      (c)  $\frac{1}{e}$       (d) -1

**20. Ans: (b)**

**Sol:** Given  $f(x,y,z) = e^{1-x\cos y} + xze^{-\frac{1}{1+y^2}}$

and  $(x, y, z) = (1, 0, e)$

$$f_x = \frac{\partial f}{\partial x} = e^{1-x\cos y} (-\cos y) + z.e^{-\frac{1}{1+y^2}}$$

$$\therefore (f_x)_{(1,0,e)} = e^{1-1} (-\cos 0) + (e).e^{-\frac{1}{1+0}} = -1 + 1 = 0$$

Hence, option (b) is correct

21. A digital communication system transmits a block of N bits. The probability of error in decoding a bit is  $\alpha$ . The error event of each bit is independent of the error events of the other bits. The received block is declared erroneous if at least one of its bits is decoded wrongly. The probability that the received block is erroneous is

- (a)  $1 - \alpha^N$                       (b)  $1 - (1-\alpha)^N$   
(c)  $\alpha^N$                               (d)  $N(1-\alpha)$

**21. Ans: (b)**

**Sol:**

1	2	3	-----	N
---	---	---	-------	---

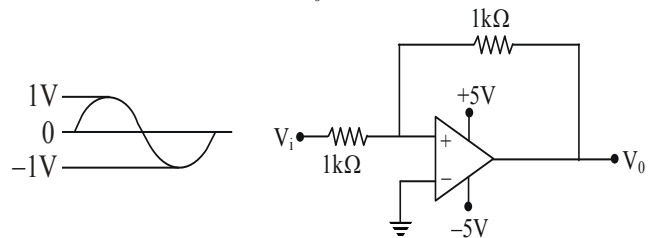
$$\begin{aligned} P(1 \text{ bit error}) &= \alpha, P(1 \text{ bit correct}) = 1 - \alpha \\ P(N \text{ bit error}) &= \alpha^N, P(N \text{ bit correct}) = (1 - \alpha)^N \end{aligned}$$

(N bits are independent)

The received block declared erroneous if atleast one of bits decoding wrongly (i.e correct probability means all bits should be correct)

$$\begin{aligned} P(\text{received block is erroneous}) &= 1 - (1 - \alpha)^N \\ &= 1 - P(\text{all bits correct}) \\ &= P(\text{any one bit or more error}) \end{aligned}$$

22. The components in the circuit shown below are ideal. If the op-amp is in positive feedback and the input voltage  $V_i$  is a sine wave of amplitude 1 V, the output voltage  $V_o$  is

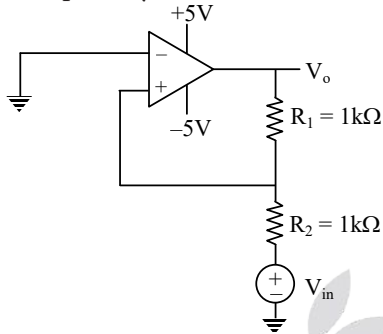


- (a) a square wave of 5V amplitude.  
(b) an inverted sine wave of 1V amplitude.  
(c) a constant of either +5 V or -5V.  
(d) a non-inverted sine wave of 2V amplitude.

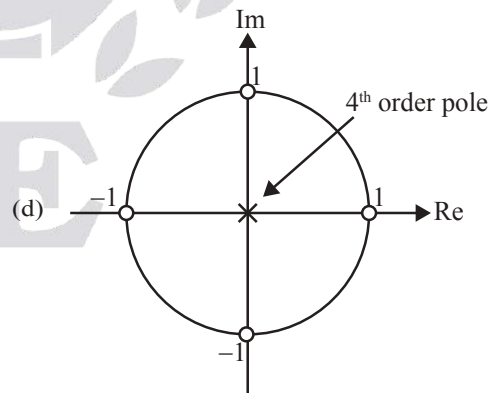
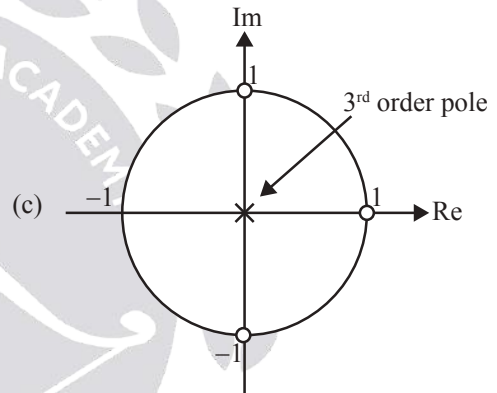
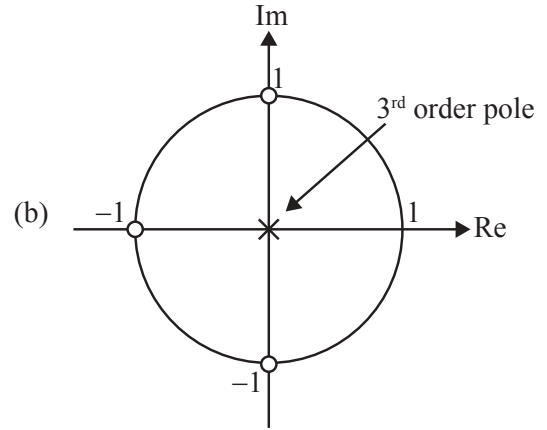
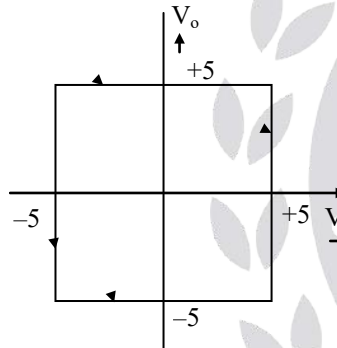
**22. Ans: (c)**

**Sol:** If  $V_{in} > +5V$  then  $V_o$  changes from  $-5V$  to  $+5V$   
 If  $V_{in} < -5V$  then  $V_o$  changes from  $+5V$  to  $-5V$   
 As  $V_{in,max} = \pm 1V$  therefore the input cannot flip the output.

So, output stays at either  $+5V$  (or)  $-5V$

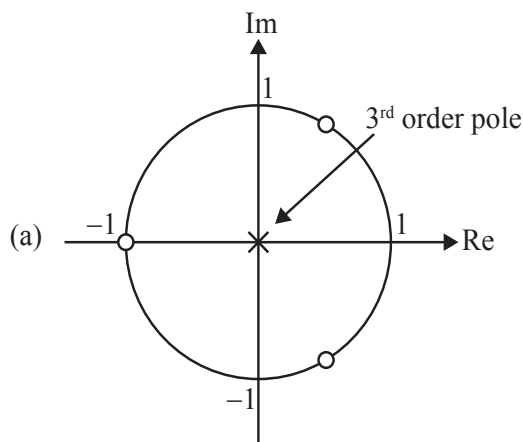


Transfer characteristics



23. Which one of the following pole-zero plots corresponds to the transfer function of an LTI system characterized by the input-output difference equation given below?

$$y[n] = \sum_{k=0}^3 (-1)^k x[n-k]$$



**23. Ans: (c)**

**Sol:**  $y(n) = \sum_{k=0}^3 (-1)^k x(n-k)$

$$y(n) = x(n) - x(n-1) + x(n-2) - x(n-3)$$

$$H(z) = \frac{Y(z)}{X(z)} = 1 - z^{-1} + z^{-2} - z^{-3}$$

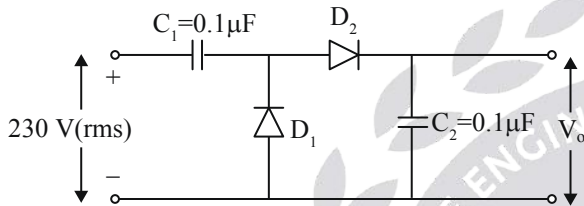
$$= \frac{z^3 - z^2 + z - 1}{z^3} = \frac{(z-1)(z^2+1)}{z^3}$$

one zero at  $z = 1$  & 2 zeros at  $z = \pm j$

3poles at  $z = 0$

From the given pole-zero plot answer will be option (c)

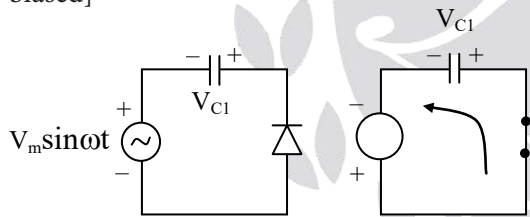
24. In the circuit shown below, all the components are ideal and the input voltage is sinusoidal. The magnitude of the steady-state output  $V_o$  (**rounded off to two decimal places**) is \_\_\_\_\_ V.



**24. Ans: 650.54**

**Sol:**  $V_{in_{max}} = 230 \times \sqrt{2} = V_m$

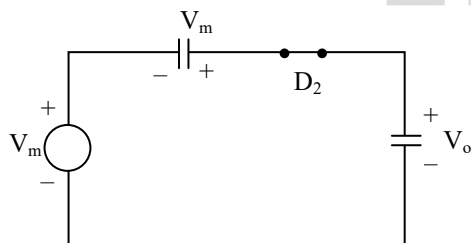
During negative cycle  $C_1$  charges [ $D_1$  forward biased]



KVL,  $-V_m + V_{C1} = 0$

$V_{C1} = V_m$

During positive cycle  $D_2$  forward biased



KVL,  $-V_m - V_m + V_o = 0$

$V_o = 2V_m$

$= 2 \times 230 \times \sqrt{2} = 650.530V$

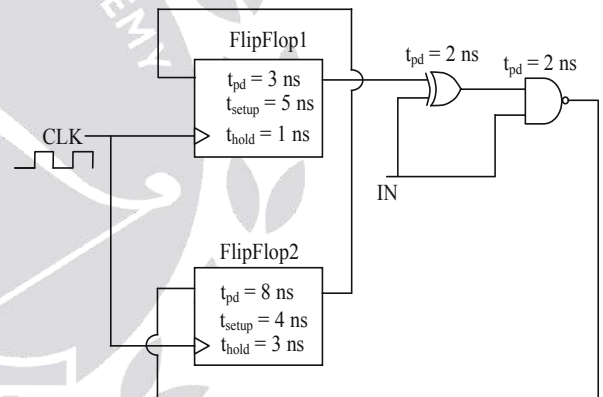
$= 650.54V.$

25. In an 8085 microprocessor, the number of address lines required to access a 16K byte memory bank is \_\_\_\_\_.

**25. Ans: 14**

**Sol:** In 8085 microprocessor, the number of address lines required to access a 16KB memory bank is  $2^n \geq 16KB \Rightarrow 2^n \geq 2^{14} \times 8$   
The number of address lines required are  $n = 14$ .

26. For the components in sequential circuit shown below,  $t_{pd}$  is the propagation delay,  $t_{setup}$  is the setup time, and  $t_{hold}$  is the hold time. The maximum clock frequency (**rounded off to the nearest integer**), at which given circuit can operate reliably is \_\_\_\_\_ MHz.



**26. Ans: 76.92**

**Sol:** In any sequential circuit, the condition for proper operation is

Clock period ( $T$ )  $\geq t_{pd} + t_{comb\ logic} + t_{setup}$

Thus,

For Flipflop 1  $\Rightarrow T \geq 8 + 5 \Rightarrow T \geq 13ns$

For Flipflop 2  $\Rightarrow T \geq 3 + 2 + 2 + 4 \Rightarrow T \geq 11ns$

Thus  $T \geq 13ns$

$\Rightarrow$  frequency of operation  $f \leq \frac{1}{13 \times 10^{-9}}$

$f_{max} = 0.07692 \times 10^9$

$f_{max} = 76.92MHz.$



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27. Which one of the following options contains two solutions of the differential equation  $\frac{dy}{dx} = (y - 1)x$ ?
- (a)  $\ln|y - 1| = 0.5x^2 + C$  and  $y = -1$   
 (b)  $\ln|y - 1| = 2x^2 + C$  and  $y = 1$   
 (c)  $\ln|y - 1| = 0.5x^2 + C$  and  $y = 1$   
 (d)  $\ln|y - 1| = 2x^2 + C$  and  $y = -1$

**27. Ans: (c)**

**Sol:** Given  $\frac{dy}{dx} = (y - 1)x$

$$\Rightarrow \int \frac{1}{y-1} dy = \int x dx + c$$

$$\Rightarrow \log|(y - 1)| = \frac{x^2}{2} + C$$

$$\left( \because \int \frac{f'(x)}{f(x)} dx = \log|f(x)| + C \right)$$

$$\therefore \log|y - 1| = (0.5)x^2 + C$$

The second solution is  $y = 1$

Hence, option (c) is correct.

28. The magnetic field of a uniform plane wave in vacuum is given by  $\vec{H}(x, y, z, t) = (\hat{a}_x + 2\hat{a}_y + b\hat{a}_z) \cos(\omega t + 3x - y - z)$ . The value of b is \_\_\_\_\_.

**28. Ans: 1**

**Sol:**  $\vec{H} = (\hat{x} + 2\hat{y} + b\hat{z}) \cos(\omega t + 3x - y - z)$

$$\vec{H} = \vec{H}_0 \cos(\omega t - \vec{k} \cdot \vec{r})$$

$$= \vec{H}_0 \cos[\omega t - (-3\hat{x} + \hat{y} + \hat{z}) \cdot (x\hat{x} + y\hat{y} + z\hat{z})]$$

$$\text{So } \vec{H}_0 = \hat{x} + 2\hat{y} + b\hat{z}$$

$$\vec{k} = -3\hat{x} + \hat{y} + \hat{z}$$

$$\text{For plane wave } \vec{H}_0 \cdot \hat{k} = 0$$

$$(\hat{x} + 2\hat{y} + b\hat{z}) \cdot \frac{(-3\hat{x} + \hat{y} + \hat{z})}{\sqrt{9+1+1}} = 0$$

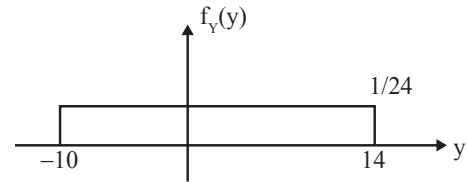
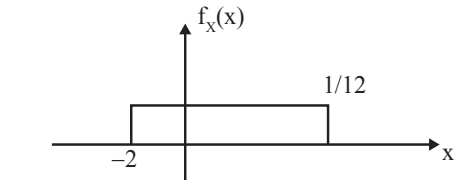
$$-3 + 2 + b = 0$$

$$b = 1$$

29. If X is a random variable with uniform probability density function in the interval  $[-2, 10]$ . For  $Y = 2X - 6$ , the conditional probability  $P(y \leq 7 | x \geq 5)$  (rounded off to three decimal places) is \_\_\_\_\_.

**29. Ans: 0.3**

**Sol:**

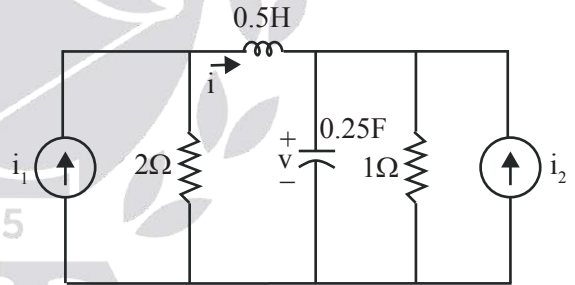


$$P(Y \leq 7 | X \geq 5) = P(Y \leq 7 | Y \geq 4)$$

$$= \frac{P(Y \leq 7, Y \geq 4)}{P(Y \geq 4)}$$

$$= \frac{P(4 \leq Y \leq 7)}{P(Y \geq 4)} = \frac{\int_4^7 1/24 dy}{\int_4^{14} 1/24 dy} = \frac{3/24}{10/24} = 0.3$$

30. For the given circuit, which one of the following is the correct state equation?



(a)  $\frac{d}{dt} \begin{bmatrix} v \\ i \end{bmatrix} = \begin{bmatrix} -4 & -4 \\ -2 & -4 \end{bmatrix} \begin{bmatrix} v \\ i \end{bmatrix} + \begin{bmatrix} 4 & 0 \\ 0 & 4 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$

(b)  $\frac{d}{dt} \begin{bmatrix} v \\ i \end{bmatrix} = \begin{bmatrix} -4 & -4 \\ -2 & 4 \end{bmatrix} \begin{bmatrix} v \\ i \end{bmatrix} + \begin{bmatrix} 4 & 4 \\ 4 & 0 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$

(c)  $\frac{d}{dt} \begin{bmatrix} v \\ i \end{bmatrix} = \begin{bmatrix} -4 & 4 \\ -2 & -4 \end{bmatrix} \begin{bmatrix} v \\ i \end{bmatrix} + \begin{bmatrix} 0 & 4 \\ 4 & 0 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$

(d)  $\frac{d}{dt} \begin{bmatrix} v \\ i \end{bmatrix} = \begin{bmatrix} 4 & -4 \\ -2 & -4 \end{bmatrix} \begin{bmatrix} v \\ i \end{bmatrix} + \begin{bmatrix} 0 & 4 \\ 4 & 4 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$

**30. Ans: (c)**

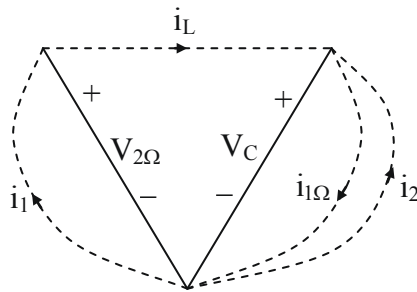
**Sol: Using Topology:**

Inductor  $\rightarrow$  Link

Capacitor  $\rightarrow$  Twigs



Current sources → Links



By KCL,

$$i_L + i_z = C \frac{dV_C}{dt} + i_{1\Omega} \quad (1)$$

By KVL,

$$-V_{2\Omega} + L \frac{di_L}{dt} + V_C = 0 \quad (2)$$

Now, voltage across  $2\Omega$ , current theory  $1\Omega$

$$i_1 = \frac{V_{2\Omega}}{2} + i_L \Rightarrow V_{2\Omega} = 2[i_1 - i_L] \quad (3)$$

$$1. i_{1\Omega} - V_C = 0 \Rightarrow i_{1\Omega} = V_C \quad (4)$$

$$i_L + i_2 = \frac{1}{4} \left[ \frac{dV_C}{dt} \right] + V_C$$

$$- [2(i_1 - i_L)] + \frac{1}{2} \frac{di_L}{dt} + V_C = 0$$

$$\frac{1}{4} \frac{dV_C}{dt} = -V_C + i_L + i_2$$

$$\frac{1}{2} \frac{di_L}{dt} = -V_C - 2i_L + 2i_1$$

$$\frac{dV_C}{dt} = -4V_C + 4i_L + 4i_2$$

$$\frac{di_L}{dt} = -2V_C - 4i_L + 4i_1$$

$$\begin{bmatrix} \frac{dV_C}{dt} \\ \frac{di_L}{dt} \end{bmatrix} = \begin{bmatrix} -4 & 4 \\ -2 & -4 \end{bmatrix} \begin{bmatrix} V_C \\ i_L \end{bmatrix} + \begin{bmatrix} 0 & 4 \\ 4 & 0 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$$

31. The characteristic equation of a system is

$$s^3 + 3s^2 + (K + 2)s + 3K = 0.$$

In the root locus plot for the given system, as  $K$  varies from 0 to  $\infty$ , the break-away or break-in point(s) lie within

- (a)  $(-2, -1)$
- (b)  $(-\infty, -3)$

(c)  $(-3, -2)$

(d)  $(-1, 0)$

**31. Ans: (d)**

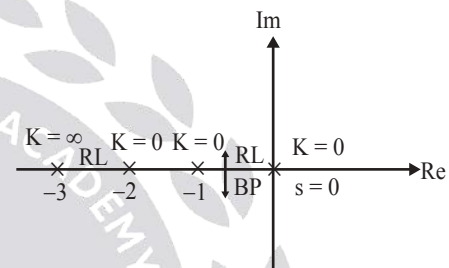
**Sol: Characteristic Equation:**

$$s^3 + 3s^2 + (K + 2)s + 3K = 0$$

$$s^3 + 3s^2 + 2s + Ks + 3K = 0$$

$$s(s^2 + 3s + 2) + K(s + 3) = 0$$

$$G(s)H(s) = \frac{K(s + 3)}{s(s + 1)(s + 2)}$$



Break point exist between  $(-1, 0)$

32. In a digital communication system, a symbol  $S$  randomly chosen from the set  $\{s_1, s_2, s_3, s_4\}$  is transmitted. It is given that  $s_1 = -3, s_2 = -1, s_3 = +1$  and  $s_4 = +2$ . The received symbol is  $Y = S + W$ .  $W$  is a zero-mean unit-variance Gaussian random variable and is independent of  $S$ .  $P_i$  is the conditional probability of symbol error for the maximum likelihood (ML) decoding when the transmitted symbol  $S = s_i$ . The index  $i$  for which the conditional symbol error probability  $P_i$  is the highest is \_\_\_\_\_.

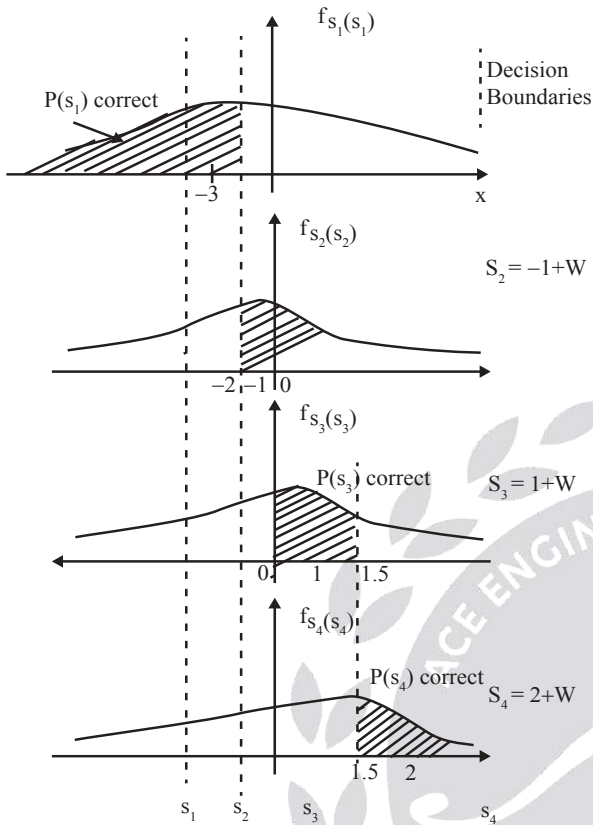
**32. Ans: 3**

**Sol:**  $S_1 = -3, S_2 = -1, S_3 = +1, S_4 = +2$

$$Y = S + W$$

$$W = N(0, 1) = \frac{1}{\sqrt{2\pi}} e^{-\omega^2/2}$$

$$f_{s_1}(s_1) \Rightarrow -3 + W = S_1$$



Since all symbols are equally likely, decision boundaries are mid points.

i.e., for  $S_1$ , decision boundary  $-2$  V i.e., anything below  $-2$  V considered as  $S_1$ .

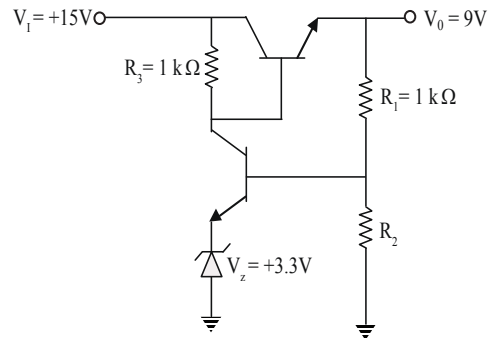
For  $S_2$  decision boundaries are  $-2$  &  $0$  V, i.e., any thing  $-2$  V to  $0$  V considered as  $S_2$ .

For  $S_3$  decision boundaries are  $0$  V &  $1.5$  V.

For  $S_4$  decision boundaries is  $1.5$  V i.e.,  $1.5$  V to  $\infty$  considered as  $S_4$ .

$P(\text{Correct symbol receiving is less for } S_3 \text{ only therefore } S_3 \text{ has highest conditional symbol error probability}).$

33. In the voltage regulator shown below,  $V_1$  is the unregulated input at  $15$  V. Assume  $V_{BE} = 0.7$  V and the base current is negligible for both the BJTs. If the regulated output  $V_0$  is  $9$  V, the value of  $R_2$  is \_\_\_\_\_  $\Omega$ .



33. Ans: 800

Sol:  $V_{R2} = 0.7 + 3.3 = 4$  V

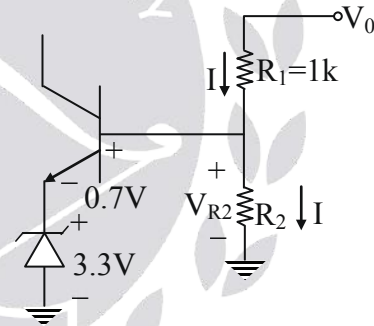
$$V_o = IR_1 + IR_2$$

$$9 = I(R_1 + R_2) \text{ [Given } V_o = 9\text{V]}$$

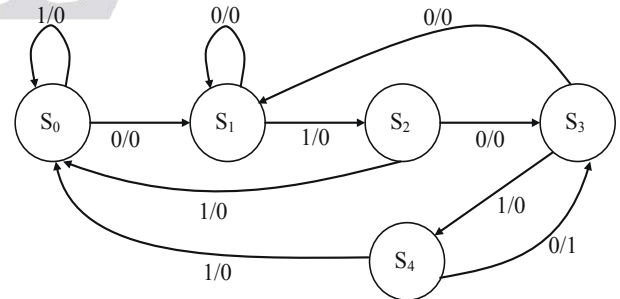
Neglect base current

$$9 = \frac{4}{R_2}(1k + R_2)$$

$$R_2 = 800\Omega$$



34. The state diagram of a sequence detector is shown below. State  $S_0$  is the initial state of sequence detector. If the output is 1, then



- (a) the sequence 01011 is detected.
- (b) the sequence 01001 is detected.
- (c) the sequence 01010 is detected.
- (d) the sequence 01110 is detected.



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**34. Ans: (c)**

**Sol:** Given  $S_0$  is initial state

For output to be 1, the sequence of states traversed are

$$S_0, S_1, S_2, S_3, S_4, S_3$$

i.e., input is  $\rightarrow 0 \ 1 \ 0 \ 1 \ 0$

**35.** A system with transfer function  $G(s) = \frac{1}{(s+1)(s+a)}$ ,  $a > 0$  is subjected to an input  $5\cos 3t$ . The steady state output of the system is  $\frac{1}{\sqrt{10}} \cos(3t - 1.892)$ . The value of  $a$  is \_\_\_\_\_.

**35. Ans: 4**

**Sol:**  $G(s) = \frac{1}{(s+1)(s+a)}$

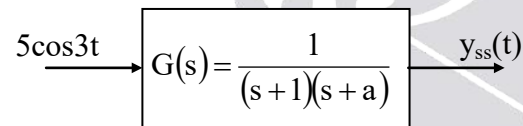
$$x(t) = 5 \cos 3t$$

$$y_{ss}(t) = \frac{1}{\sqrt{10}} \cos(3t - 1.892)$$

$$x(t) = A \cos(\omega_0 t + \theta)$$

$$H(s)|_{s=j\omega_0} = |H(\omega_0)| \angle H(\omega_0)$$

$$y_{ss}(t) = A |H(\omega_0)| \cos(\omega_0 t + \theta + \angle H(\omega_0))$$



$$A = 5 \quad \omega_0 = 3$$

$$G(s)|_{s=j3} = \frac{1}{(j3+1)(j3+a)}$$

$$|G(j3)| = \frac{1}{\sqrt{a^2 + 9} \sqrt{1 + 9}}$$

From the above expression

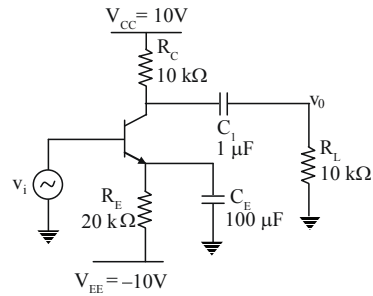
$$A |G(\omega_0)| = \frac{1}{\sqrt{10}}$$

$$\frac{5}{\sqrt{10} \sqrt{a^2 + 9}} = \frac{1}{\sqrt{10}} \Rightarrow 5 \sqrt{a^2 + 9}$$

$$\begin{aligned} 25 - a^2 + 9 \\ a = 4 \end{aligned}$$

**36.** For the BJT in the amplifier shown below,  $V_{BE} = 0.7V$ ,  $kT/q = 26 \text{ mV}$ . Assume that BJT output resistance ( $r_o$ ) is very high and the base current is negligible. The capacitors are also assumed to be

short circuited at signal frequencies. The input  $v_i$  is direct coupled. The low frequency voltage gain  $v_o/v_i$  of the amplifier is



(a) - 89.42

(b) - 256.42

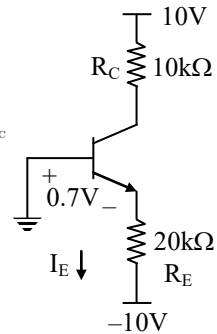
(c) - 178.85

(d) - 128.21

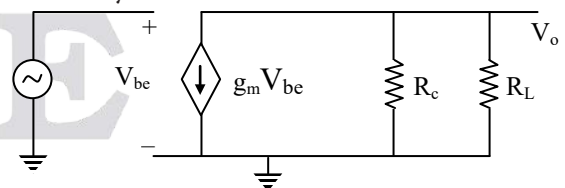
**36. Ans: (a)**

**Sol:** DC Analysis:

$$\begin{aligned} I_E &= \frac{-0.7 - (-10V)}{20k} \\ &= \frac{9.3V}{20V} = 0.465mA = I_{C_{DC}} \\ g_m &= \frac{I_{C_{DC}}}{V_t} = 0.0178 \end{aligned}$$



AC Analysis:



$$V_o = -g_m (R_C || R_L) V_{be}$$

$$V_i = V_{be}$$

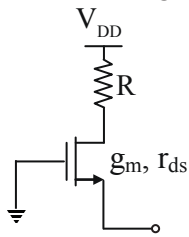
$$\frac{V_o}{V_i} = \frac{-g_m (R_C || R_L) V_{be}}{V_{be}} = -g_m (R_C || R_L)$$

$$= -0.0178(10k || 10k)$$

$$= -0.0178(5k)$$

$$= -89.423$$

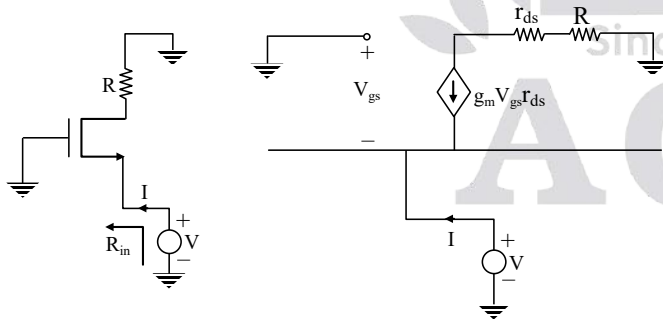
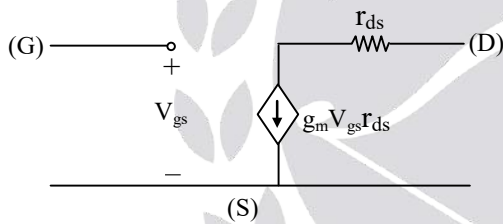
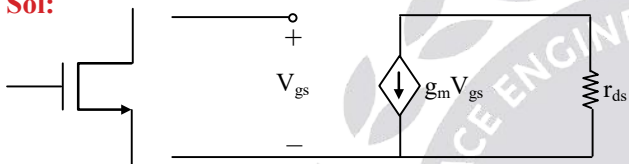
37. Using the incremental low frequency small-signal model of the MOS device, the Norton equivalent resistance of the following circuit is



- (a)  $\frac{r_{ds} + R}{1 + g_m r_{ds}}$       (b)  $r_{ds} + R$   
 (c)  $r_{ds} + R + g_m r_{ds} R$       (d)  $r_{ds} + \frac{1}{g_m} + R$

**37. Ans: (a)**

**Sol:**



KVL

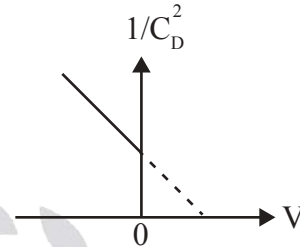
$$V_{gs} + V = 0 \Rightarrow V = -V_{gs}$$

$$I = \frac{V_x}{r_{ds} + R} = \frac{-g_m r_{ds} V_{gs} + V}{r_{ds} + R}$$

$$I = \frac{g_m r_{ds} V + V}{r_{ds} + R}$$

$$\frac{V}{I} = \frac{r_{ds} + R}{1 + g_m r_{ds}}$$

38. A one-sided abrupt pn junction diode has a depletion capacitance  $C_D$  of 50 pF at a reverse bias of 0.2V. The plot of  $1/C_D^2$  versus the applied voltage V for this diode is a straight line as shown in the figure below. The slope of the plot is \_\_\_\_\_  $\times 10^{20} \text{ F}^{-2} \text{ V}^{-1}$ .



- (a) -5.7      (b) -0.4  
 (c) -1.2      (d) -3.8

**38. Ans: (\*) insufficient data**

**Sol:** [If we assume  $V_0 = 0.5\text{V}$ ]

$$C_D = \sqrt{\frac{q\epsilon}{2(V_0 + V_R)} \left( \frac{N_A N_D}{N_A + N_D} \right)}$$

$$C_D^2 \propto \frac{1}{(V_0 + V_R)}$$

$$\frac{1}{C_D^2} \propto (V_0 + V_R)$$

$$\frac{1}{C_D^2} = k(V_0 + V_R)$$

$$k = \frac{\frac{1}{C_D^2}}{V_0 + V_R} = \text{slope}$$

$$= \frac{\left( \frac{1}{50\text{pF}} \right)^2}{0.5 + 0.2}$$

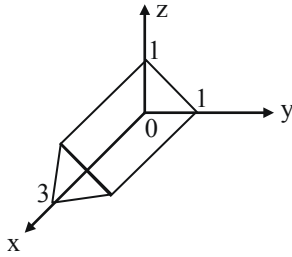
$$= \frac{1}{(50\text{pF})^2 \times 0.7}$$

$$= 5.71 \times 10^{20} \text{ F}^{-2} \text{ V}^{-1}$$

Then option (a) is correct

39. For the solid S shown below, the value of  $\iiint_S x dx dy dz$

(rounded off to two decimal places) is



**39. Ans: (2.25)**

**Sol:** From the figures, the limits of the integral are given by

$$\lim \text{its: } \begin{cases} x = 0 \text{ to } x = 3 \\ y = 0 \text{ to } y = 1 \\ z = 0 \text{ to } z = 1 - y \end{cases}$$

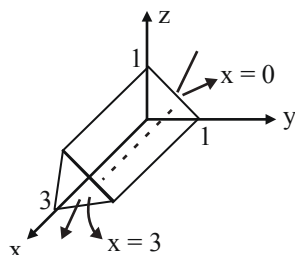
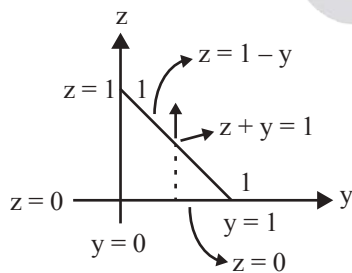
$$I = \int_{x=0}^3 \left[ \int_{y=0}^1 \left\{ \int_{z=0}^{1-y} x dz \right\} dy \right] dx$$

$$= \int_{x=0}^3 \left[ \int_{y=0}^1 x(z)_0^{1-y} dy \right] dx$$

$$= \int_{x=0}^3 \left[ \int_{y=0}^1 x \cdot (1-y) dy \right] dx$$

$$= \left( \frac{x^2}{2} \right)_0^3 \cdot \left( y - \frac{y^2}{2} \right)_0^1$$

$$= \frac{9}{4} = 2.25$$

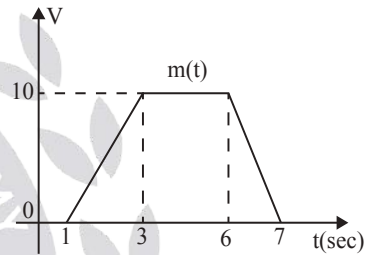


40.  $S_{PM}(t)$  and  $S_{FM}(t)$  as defined below, are the phase modulated and the frequency modulated waveforms, respectively, corresponding to the message signal  $m(t)$  shown in the figure.

$$S_{PM}(t) = \cos(1000\pi t + K_p m(t))$$

$$\text{and } S_{FM}(t) = \cos\left(1000\pi t + K_f \int_{-\infty}^t m(\tau) d\tau\right)$$

where  $K_p$  is the phase deviation constant in radians/volt and  $K_f$  is the frequency deviation constant in radians/second/volt. If the highest instantaneous frequencies of  $S_{PM}(t)$  and  $S_{FM}(t)$  are same, then the value of the ratio  $\frac{K_p}{K_f}$  is \_\_\_\_\_ seconds.



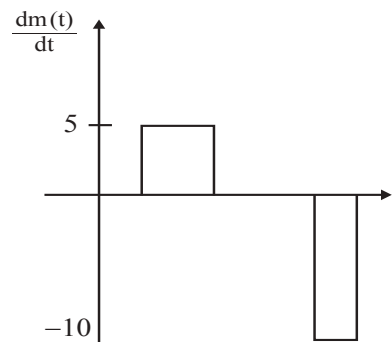
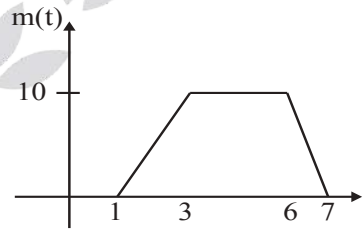
**40. Ans: 2**

**Sol:** highest instantaneous frequencies are same.

$$\text{i.e., } f_{i, \max, PM} = f_{i, \max, FM}$$

$$f_c + \frac{K_p}{2\pi} \frac{dm(t)}{dt} \Big|_{\max} = f_c + \frac{K_f}{2\pi} m(t) \Big|_{\max}$$

$$K_p \frac{dm(t)}{dt} \Big|_{\max} = K_f m(t) \Big|_{\max}$$



$$K_p \cdot 5 = K_f \cdot 10$$

$$\frac{K_p}{K_f} = \frac{10}{5} = 2 \text{ sec}$$



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41. A p-n junction solar cell of area  $1.0 \text{ cm}^2$ , illuminated uniformly with  $100 \text{ mW cm}^{-2}$ , has the following parameters: Efficiency = 15%, open circuit voltage =  $0.7 \text{ V}$ , fill factor = 0.8, and thickness =  $200 \mu\text{m}$ . The charge of an electron is  $1.6 \times 10^{-19} \text{ C}$ . The average optical generation rate (in  $\text{cm}^{-3} \text{ s}^{-1}$ ) is
- (a)  $83.60 \times 10^{19}$       (b)  $1.04 \times 10^{19}$   
 (c)  $5.57 \times 10^{19}$       (d)  $0.84 \times 10^{19}$

**41. Ans: (d)**

**Sol:**  $A = 1 \text{ cm}^2$

$$P_{in} (/cm^2) = 100 \text{ mW/cm}^2$$

$$\eta = 0.15, V_{oc} = 0.7, \text{ Fill factor} = 0.8$$

$$\text{Thickness} = 200 \mu\text{m}$$

$$\text{Power} (/cm^2) = \frac{100 \text{ mW/cm}^2}{200 \times 10^{-4}} = 5 \text{ W/cm}^3$$

$$\eta = \frac{V_m I_m}{P_{in}} \text{ Fill factor} = \frac{V_m I_m}{V_{oc} I_{sc}}$$

$$V_m I_m = \eta P_{in}$$

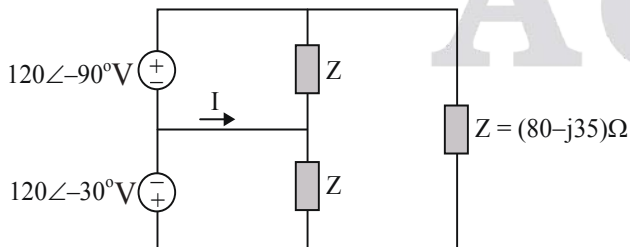
$$I_{sc} = \frac{V_m I_m}{V_{oc} (\text{Fill Factor})} = \frac{0.75}{0.7 \times 0.8} = 1.339 \text{ A/cm}^3$$

$$I = \frac{Q}{t} \Rightarrow Q = It = 1.339 \text{ A} \cdot \text{s/cm}^3$$

$$Q = nq \Rightarrow n = \frac{Q}{q} = \frac{1.339 \text{ C/cm}^2}{1.6 \times 10^{-19} \text{ C}} = 0.84 \times 10^{19} / \text{cm}^3$$

$$\text{Optical generation rate} = 0.84 \times 10^{19} / \text{Cm}^3 \cdot \text{s}$$

42. The current  $I$  in the given network is

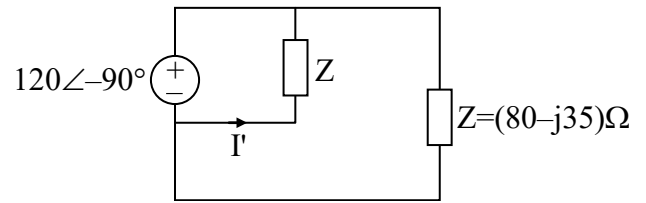


- (a)  $2.38 \angle -23.63^\circ \text{ A}$   
 (b)  $2.38 \angle -96.37^\circ \text{ A}$   
 (c)  $2.38 \angle 143.63^\circ \text{ A}$   
 (d)  $0 \text{ A}$

**42. Ans: (c)**

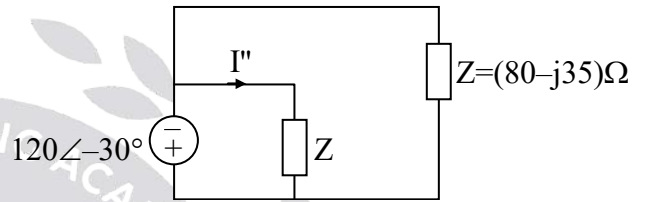
**Sol:** By applying super-position theorem

Step-I



$$I' = -\frac{[120 \angle -90^\circ]}{Z} = -\frac{[-j120]}{80-j35} = \frac{j120}{80-j35}$$

Step-II



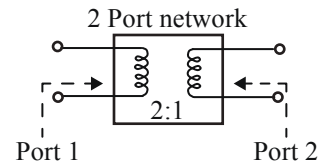
$$I'' = -\frac{[120 \angle -30^\circ]}{Z} = \frac{-[120 \angle -30^\circ]}{80-j35}$$

$$I = I' + I'' = \frac{1}{(80-j35)} [j120 - 103.92 + j60]$$

$$I = \frac{(-103.92 + j180)}{(80-j35)} = \frac{207.34 \angle 120^\circ}{87.32 \angle 23.63^\circ}$$

$$I = 2.380 \angle 143.63^\circ \text{ A}$$

43. For a 2-port network consisting of an ideal lossless transformer, the parameter  $S_{21}$  (**rounded off to two decimal places**) for a reference impedance of  $10 \Omega$ , is \_\_\_\_\_.



**43. Ans: 0.8**

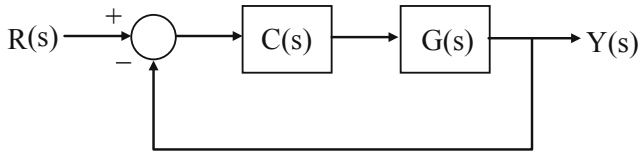
**Sol:** For ideal Transformer,

$$\begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} = \begin{bmatrix} \frac{n^2-1}{n^2+1} & \frac{2n}{n^2+1} \\ \frac{2n}{n^2+1} & \frac{1-n^2}{n^2+1} \end{bmatrix}$$

$$\therefore n = 2 \Rightarrow S_{12} = S_{21} = \frac{2n}{n^2+1} = \frac{2 \times 2}{2^2+1} = 0.8$$



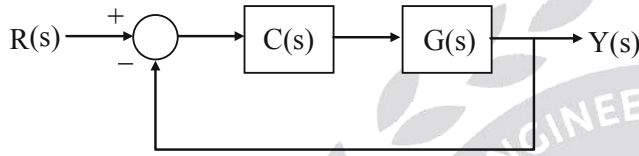
44. Consider the following closed loop control system



where  $G(s) = \frac{1}{s(s+1)}$  and  $C(s) = K \frac{s+1}{s(s+3)}$ .  
If the steady state error for a unit ramp input is 0.1, then the value of K is \_\_\_\_.

**44. Ans: 30**

**Sol:**



$$C(s)G(s) = \frac{k(s+1)}{s(s+1)(s+3)} = \frac{k}{s(s+3)}$$

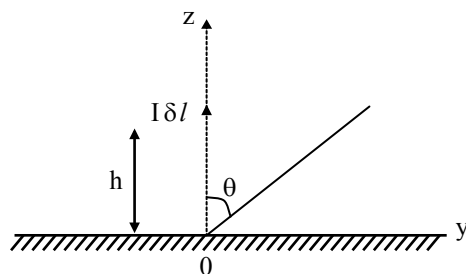
$$e_{ss}(\text{ramp}) = \frac{1}{k_v} = 0.1$$

$$k_v = \lim_{s \rightarrow 0} s C(s)G(s) = \lim_{s \rightarrow 0} s \cdot \frac{k}{s(s+3)} = \frac{k}{3}$$

$$e_{ss} = \frac{1}{k_v} = \frac{3}{k} = 0.1$$

$$k = 30$$

45. For an infinitesimally small dipole in free space, the electric field  $E_\theta$  in the far field is proportional to  $\left(\frac{e^{-jkr}}{r}\right) \sin \theta$ , where  $k = \frac{2\pi}{\lambda}$ . A vertical infinitesimally small electric dipole ( $\delta l \ll \lambda$ ) is placed at a distance  $h$  ( $h > 0$ ) above an infinite ideal conducting plane, as shown in figure. The minimum value of 'h', for which one of the maxima in the far field radiation pattern occurs at  $\theta = 60^\circ$  is \_\_\_\_.



Infinite conduction plate

(a)  $\lambda$  (b)  $0.25\lambda$

(c)  $0.75\lambda$  (d)  $0.5\lambda$

**45. Ans: (a)**

**Sol:** Consider an infinitesimal electric dipole

(of length  $\lambda$ ), which is vertically placed at height 'h' above an infinite grounded conductor.

The resultant electric field intensity is given by

$$E_\theta = \frac{j\eta I_0 \beta d l \sin \theta}{4\pi r} e^{-j\beta r} 2 \cos(\beta h \cos \theta); z \geq 0$$

$$= 0 \quad ; z < 0$$

(or)

$$E_\theta = \frac{j\eta I_0 k d l \sin \theta}{4\pi r} e^{-jkr} 2 \cos(kh \cos \theta); z \geq 0$$

$$= 0 \quad ; z < 0$$

where k (or)  $\beta$  is phase shift constant (or) wave number.

$$\beta(\text{or})k = \frac{2\pi}{\lambda}$$

Given  $\theta_{\max} = 60^\circ$

Field will have maxima,

when  $|\cos(kh \cos \theta_{\max})| = 1$

$$\Rightarrow kh \cos \theta_{\max} = \pi$$

$$\frac{2\pi}{\lambda} h \cos 60^\circ = \pi$$

$$\frac{2\pi}{\lambda} \cdot h \cdot \frac{1}{2} = \pi$$

$$\therefore h = \lambda$$

(or)

$$\frac{\partial E_\theta}{\partial h} = 0$$

$$\text{let } \frac{j\eta k I_0 d l e^{-jkr} \sin \theta}{4\pi r} = P$$

$$\frac{\partial}{\partial h} \{2P \cos(kh \cos \theta_{\max})\} = 0$$

$$-2pk \cos \theta_{\max} \sin(kh \cos \theta_{\max}) = 0$$

$$\sin(kh \cos \theta_{\max}) = 0$$

$$kh \cos \theta_{\max} = n\pi$$

assume  $n = 1$

$$kh \cos 60^\circ = \pi$$

$$\frac{2\pi}{\lambda} \times h \cdot \frac{1}{2} = \pi$$

$$\therefore h = \lambda$$



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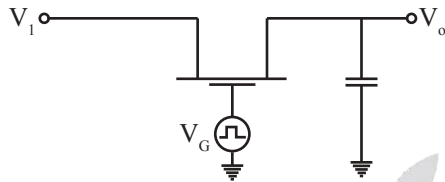
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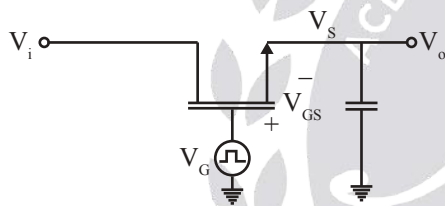
46. An enhancement MOSFET of threshold voltage 3 V is being used in the sample and hold circuit given below. Assume that the substrate of the MOS device is connected to -10 V. If the input voltage  $V_i$  lies between  $\pm 10$  V, the minimum and the maximum values of  $V_G$  required for proper sampling and holding respectively, are



- (a) 13 V and -7V. (b) 10 V and -13 V.  
(c) 10 V and -10 V. (d) 3 V and -3 V.

**46. Ans: (a)**

**Sol:**



$$V_T = 3V$$

$$V_i = \pm 10V$$

During sampling (i.e when input  $\pm 10V$ )

MOSFET must be ON:

$$V_{GS} > V_T$$

$$V_G - V_s > V_T \quad [\because V_{GS} = V_G - V_s]$$

$$V_G > V_s + V_T$$

$$V_G > V_i + V_T$$

$$\text{when } V_i = 10V \Rightarrow V_G > 10V + 3V$$

$$[\text{when } V_{i_{\max}} = 10V]$$

$$V_G > 13V$$

$$\text{when } V_i = -10V$$

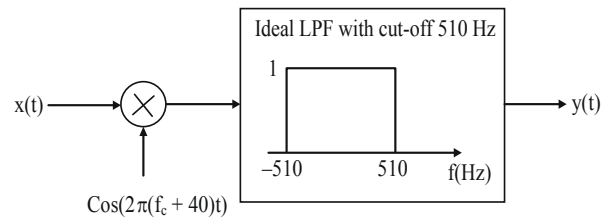
$$\Rightarrow V_G > V_i + V_T \quad [\text{when } V_{i_{\min}} = -10V]$$

$$V_G > -10 + 3V$$

$$V_G > -7V$$

47. For the modulated signal  $x(t) = m(t)\cos(2\pi f_c t)$ , the message signal  $m(t) = 4\cos(1000\pi t)$  and the carrier

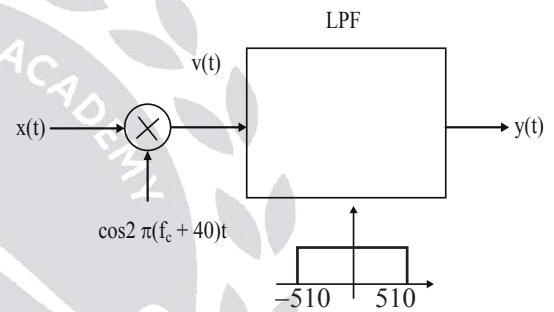
frequency  $f_c$  is 1 MHz. The signal  $x(t)$  is passed through a demodulator, as shown in the figure below. The output  $y(t)$  of the demodulator is



- (a)  $\cos(540\pi t)$  (b)  $\cos(920\pi t)$   
(c)  $\cos(460\pi t)$  (d)  $\cos(1000\pi t)$

**47. Ans: (b)**

**Sol:**



$$v(t) = m(t) \cos(2\pi f_c t) \cos(2\pi (f_c + 40)t)$$

$$v(t) = 4 \cos(2\pi 500t) \cos(2\pi \cdot 10^6 t) \cos(2\pi (10^6 + 40)t)$$

$$v(t) = 4 \cos(2\pi 500t) \frac{1}{2} [\cos(4\pi 10^6 + 2\pi 40)t + \cos(2\pi 40t)]$$

$$v(t) = 2 \cos(2\pi \cdot 500t) [\cos(2\pi \cdot 40t) + \cos(2\pi (2 \cdot 10^6 + 40)t)]$$

$$v(t) = \cos(2\pi \cdot 540t) + \cos(2\pi \cdot 460t) + \cos(2\pi (2 \cdot 10^6 + 540)t) + \cos(2\pi (2 \cdot 10^6 + 460)t)$$

$$y(t) = \cos(2\pi 460t)$$

$$y(t) = \cos(920\pi t)$$

48. A finite duration discrete time signals  $x[n]$  is obtained by sampling the continuous time signal  $x(t) = \cos(200\pi t)$  of sample instant  $t = \frac{n}{400}$ ,  $n = 0, 1, 2, \dots, 7$ . The 8-point discrete fourier transform (DFT) of  $x(n)$  is defined as

$$X[k] = \sum_{n=0}^7 x(n) \cdot e^{-j\frac{\pi k n}{4}}, k = 0, 1, \dots, 7$$

Which one of the following statements is TRUE?

- (a) Only  $X(2)$  and  $X(6)$  are non-zero  
(b) Only  $X(3)$  and  $X(5)$  are non-zero

- (c) Only X(4) is non-zero  
(d) All X(k) are non-zero

**48. Ans: (a)**

**Sol:**  $x(t) = \cos(200\pi t)$

$$x(nT_s) = \cos\left(\frac{200\pi n}{400}\right) \Rightarrow x(n) = \cos\left(\frac{\pi n}{2}\right)$$

$$x(n) = \{1, 0, -1, 0, 1, 0, -1, 0\}$$

$$X(k) = \sum_{n=0}^{N-1} x(n)W_N^{kn}$$

$$= \sum_{n=0}^7 x(n)e^{-j\frac{\pi kn}{4}}$$

$$X(4) = \sum_{n=0}^7 x(n)e^{-j\pi n} = \sum_{n=0}^7 x(n)(-1)^n$$

$$X(4) = 1 - 1 + 1 - 1 = 0$$

$$X(2) = \sum_{n=0}^7 x(n)e^{-j\frac{\pi n}{2}} = 1 + 1 + 1 + 1 = 4$$

As  $X(k) = X^*(N - k)$

$$X(2) = X^*(8-2) = X^*(6)$$

Only X(2) & (6) are non zero.

**(or)**

when we look at x(n), it contains only even samples. If we assume  $z(n) = \{1-1 \ 1-1\}$

$$Z(k) = \begin{bmatrix} Z(0) \\ Z(1) \\ Z(2) \\ Z(3) \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 \\ 1 & -j & -1 & j \\ 1 & -1 & 1 & -1 \\ 1 & j & -1 & -j \end{bmatrix} \begin{bmatrix} 1 \\ -1 \\ 1 \\ -1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 4 \\ 0 \end{bmatrix}$$

We know zero interpolation in time domain corresponds to replication of DFT spectrum

$$x(n) = z\left(\frac{n}{2}\right) \xrightarrow{\text{DFT}} X(k) = \{Z(k), Z(k)\}$$

$$= \{0,0,4,0,0,0,4,0\}$$

**(or)**

$$\cos\left(\frac{2\pi}{N}k_0n\right) \leftrightarrow \frac{N}{2}[\delta(k - k_0) + \delta(k + k_0)]$$

$$\cos\left(\frac{n\pi}{2}\right) = \cos\left(\frac{2\pi}{8}2n\right) \leftrightarrow \frac{8}{2}[\delta(k - 2) + \delta(k + 2)]$$

So, non zero samples are -2, 2. From periodicity property non zero samples are -2+8, 2 = 6,2.

49. The transfer function of a stable discrete time LTI system is  $H(z) = \frac{K(z - \alpha)}{(z + 0.5)}$ , where K and  $\alpha$  are real numbers. The value of  $\alpha$  (rounded off to one decimal place) with  $|\alpha| > 1$ , for which the magnitude response of the system is constant over all frequencies, is \_\_\_\_.

**49. Ans: -2**

**Sol:**  $H(z) = \frac{K(z - \alpha)}{z + 0.5}, |\alpha| > 1$

$$|H(e^{j\omega})| = 1 \quad \forall \quad \omega$$

For an all pass filter poles & zeros are reciprocal to each other.

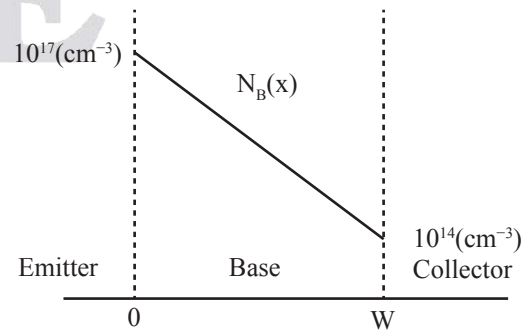
To get constant magnitude for all frequency pole located at  $z = -0.5$

$$\therefore \text{zero is located at } = \frac{1}{-0.5} = -2$$

$$H(z) = \frac{k(z + 2)}{z + 0.5}$$

$$\therefore \alpha = -2$$

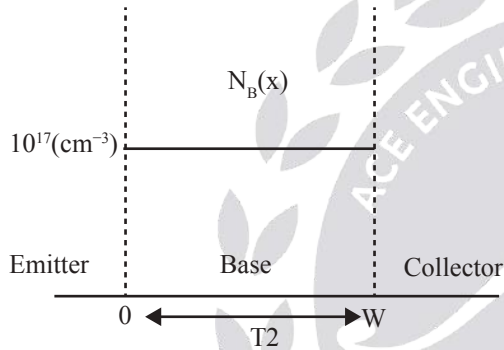
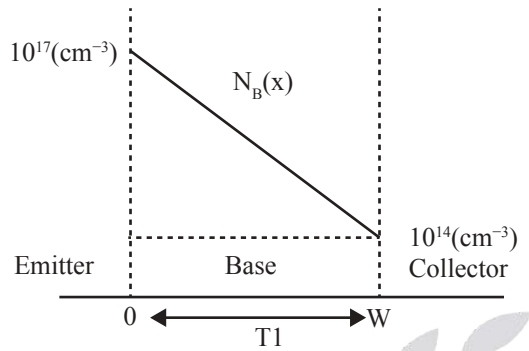
50. The base of an npn BJT T1 has a linear doping profile  $N_B(x)$  as shown below. The base of another non BJT T2 has a uniform doping  $N_B$  of  $10^{17} \text{ cm}^{-3}$ . All other parameters are identical for both the devices. Assuming that the hole density profile is the same as that of doping, the common-emitter current gain of T2 is



- (a) approximately 0.3 times that of T1.
- (b) approximately 2.0 times that of T1.
- (c) approximately 0.7 times that of T1.
- (d) approximately 2.5 times that of T1.

50. Ans: (b)

Sol:  $\beta_{T2} = \frac{\text{Area under the carrier profile of base of T1}}{\text{Area under the carrier profile of base of T2}}$

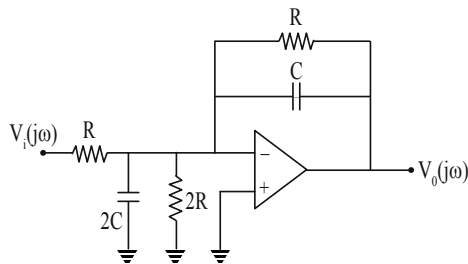


$$\beta_{T2} = \frac{10^{17} \times W}{\frac{1}{2}(10^{17} - 10^{14})W + 10^{14}W}$$

$$= \frac{10^{17}}{\frac{1}{2}(10^{17} - 10^{14}) + 10^{14}} \approx 2$$

$$\Rightarrow \beta_{T2} = 2\beta_{T1}$$

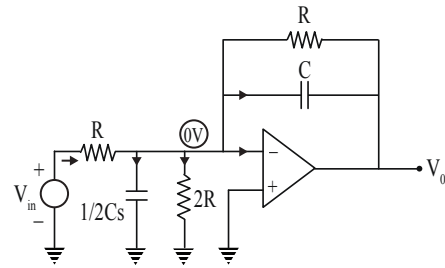
51. The components in the circuit given below are ideal. If  $R = 2 \text{ k}\Omega$  and  $C = 1 \text{ }\mu\text{F}$ , the  $-3 \text{ dB}$  cut-off frequency of the circuit in Hz is



- (a) 14.92
- (b) 59.68
- (c) 34.46
- (d) 79.58

51. Ans: (d)

Sol:



No current flows through  $2C$  and  $2R$

KCL

$$\frac{V_{in} - 0}{R} = \frac{0 - 0}{1/2sC} + \frac{0 - 0}{2R} + 0 + \frac{0 - V_o}{1/sC} + \frac{0 - V_o}{R}$$

$$\frac{V_{in}}{R} = -V_o \left[ \frac{1}{R} + sC \right]$$

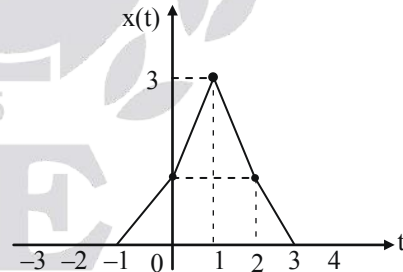
$$\left| \frac{V_o}{V_{in}} \right| = \frac{1}{1 + sCR} = \frac{1}{1 + s\tau}$$

$$\omega_{3dB} = \frac{1}{\tau} = \frac{1}{RC}$$

$$f_{3dB} = \frac{1}{2\pi RC} = \frac{1}{2\pi(2k)(1\mu)} = 79.58\text{Hz}$$

52.  $X(\omega)$  is Fourier transform of  $x(t)$  shown below.

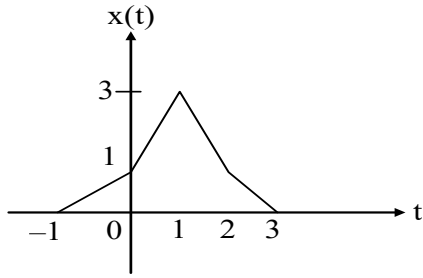
The value of  $\int_{-\infty}^{\infty} |X(\omega)|^2 d\omega$  (rounded off to two decimal places) is \_\_\_\_\_.



52. Ans: 58.64

Sol: From parseval's theorem

$$\int_{-\infty}^{\infty} |X(\omega)|^2 d\omega = 2\pi \int_{-\infty}^{\infty} |x(t)|^2 dt$$



Because of symmetry of the signal w.r.t to  $t = 1$

$$\int_{-\infty}^{+\infty} |X(\omega)|^2 d\omega = 2\pi \left[ \int_{-1}^3 |x(t)|^2 dt \right]$$

$$= 2(2\pi) \left[ \int_{-1}^0 (t+1)^2 dt + \int_0^1 (2t+1)^2 dt \right]$$

$$2(2\pi) \left[ \int_{-1}^0 (t+1)^2 dt + \int_0^1 (4t^2 + 4t + 1) dt \right]$$

$$= 4\pi \left[ \left[ \frac{(t+1)^3}{3} \right]_{-1}^0 + \left[ \frac{4t^3}{3} + \frac{4t^2}{2} + t \right]_0^1 \right]$$

$$= 4\pi \left[ \frac{1}{3} + \frac{4}{3} + 2 + 1 \right] = 4\pi \left[ \frac{5}{3} + 3 \right]$$

$$= \frac{56\pi}{3}$$

$$= 58.64$$

53. P, Q, and R are the decimal integers corresponding to the 4-bit binary number 1100 considered in signed magnitude, 1's complement and 2's complement representations, respectively. The 6-bit 2's complement representation of (P + Q + R) is

- (a) 111101
- (b) 110101
- (c) 110010
- (d) 111001

53. **Ans: (b)**

**Sol:** P = The decimal value of sign magnitude no 1100  
= -4

Q = The decimal value of 1's complement no 1100  
= -3

R = The decimal value of 2's complement no 1100  
= -4

Thus  $P+Q+R = (-4) + (-3) + (-4)$

$$P+Q+R = -11$$

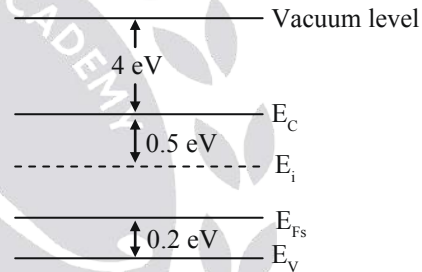
$$= 2\text{'s complement of } +11$$

$$= 2\text{'s complement of } 001011$$

$$= 110101$$

Thus P+Q+R in 6-bit 2's complement representation is 110101.

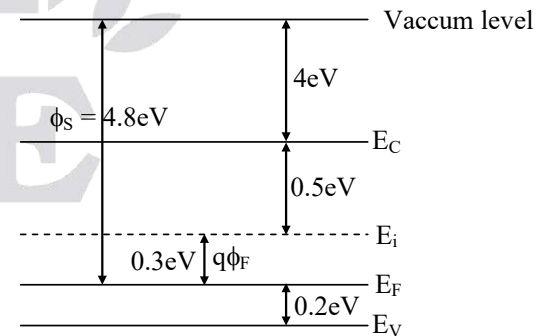
54. The band diagram of a p-type semiconductor with a band-gap of 1 eV is shown, using this semiconductor, a MOS capacitor having  $V_{TH}$  of -0.16 V,  $C'_{ox}$  of 100 nF/cm<sup>2</sup> and a metal work function of 3.87 eV is fabricated. There is no charge within the oxide. If the voltage across the capacitor is  $V_{TH}$ , the magnitude of depletion charge per unit area (in C/cm<sup>2</sup>) is



- (a)  $1.41 \times 10^{-8}$
- (b)  $1.70 \times 10^{-8}$
- (c)  $0.52 \times 10^{-8}$
- (d)  $0.93 \times 10^{-8}$

54. **Ans: (b)**

**Sol:**



$$\phi_s = 4\text{eV} + 0.5\text{eV} + 0.3\text{eV} = 4.8\text{eV}$$

$$V_{TH} = -0.16\text{V}, C'_{ox} = 100\text{nF/cm}^2$$

$$\phi_m = 3.87\text{ eV}$$

$$V_T - V_{FB} = \frac{|Q_{div}|}{C_{ox}} + \phi_t$$

$$V_{FB} = \phi_{ms} (\because \text{No oxide charge})$$

$$V_{FB} = \phi_{ms} = \phi_m - \phi_s = 3.87 - 4.8 = -0.93$$

$$\phi_t = 2 \phi_F, \phi_F = 0.3V$$

$$\phi_t = 2 \times 0.3 = 0.6V$$

$$-0.16 - (-0.93) = \frac{|Q_{div}|}{100n} + 0.6$$

$$|Q_{div}| = 0.17 \times 100 \times 10^{-9} = 17 \times 10^{-9}$$

$$= 1.7 \times 10^{-8} C/cm^2$$

55. Consider the following system of linear equation.

$$x_1 + 2x_2 = b_1; 2x_1 + 4x_2 = b_2; 3x_1 + 7x_2 = b_3;$$

$$3x_1 + 9x_2 = b_4$$

Which one of the following conditions ensures that a solution exists for the above system?

(a)  $b_2 = 2b_1$  and  $3b_1 - 6b_3 + b_4 = 0$

(b)  $b_3 = 2b_1$  and  $3b_1 - 6b_3 + b_4 = 0$

(c)  $b_3 = 2b_1$  and  $6b_1 - 3b_3 + b_4 = 0$

(d)  $b_2 = 2b_1$  and  $6b_1 - 3b_3 + b_4 = 0$

**55. Ans: (d)**

**Sol:** Consider augmented matrix

$$(A|B) = \left[ \begin{array}{cc|c} 1 & 2 & b_1 \\ 2 & 4 & b_2 \\ 3 & 7 & b_3 \\ 3 & 9 & b_4 \end{array} \right]$$

$$R_2 \rightarrow R_2 - 2R_1; R_3 \rightarrow R_3 - 3R_1; R_4 \rightarrow R_4 - 3R_1$$

$$(A|B) \sim \left[ \begin{array}{cc|c} 1 & 2 & b_1 \\ 0 & 0 & b_2 - 2b_1 \\ 0 & 1 & b_3 - 3b_1 \\ 0 & 3 & b_4 - 3b_1 \end{array} \right]$$

$$R_2 \leftrightarrow R_3$$

$$(A|B) \sim \left[ \begin{array}{cc|c} 1 & 2 & b_1 \\ 0 & 1 & b_3 - 3b_1 \\ 0 & 0 & b_2 - 2b_1 \\ 0 & 3 & b_4 - 3b_1 \end{array} \right]$$

$$R_4 \rightarrow R_4 - 3R_2$$

$$(A|B) \sim \left[ \begin{array}{cc|c} 1 & 2 & b_1 \\ 0 & 1 & b_3 - 3b_1 \\ 0 & 0 & b_2 - 2b_1 \\ 0 & 0 & 6b_1 - 3b_3 + b_4 \end{array} \right]$$

Here,  $\rho(A) = 2$

To have a solution,  $\rho(A) = 2 = \rho(A|B)$

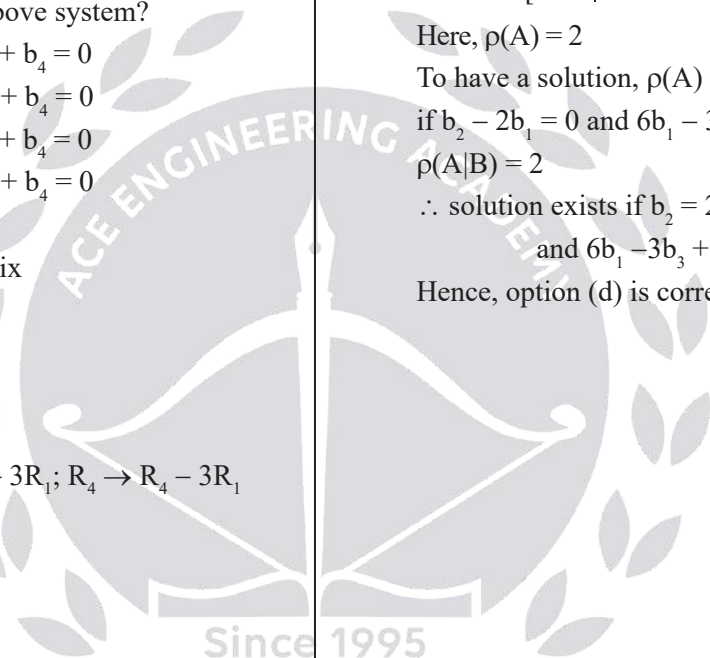
if  $b_2 - 2b_1 = 0$  and  $6b_1 - 3b_3 + b_4 = 0$  then

$$\rho(A|B) = 2$$

$\therefore$  solution exists if  $b_2 = 2b_1$

$$\text{and } 6b_1 - 3b_3 + b_4 = 0$$

Hence, option (d) is correct.



# ACE

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<b>5</b>	<b>44</b>	<b>6</b>	<b>60</b>	<b>7</b>	<b>71</b>	<b>9</b>	<b>74</b>	<b>5</b>	<b>28</b>	<b>10</b>	<b>74</b>	<b>10</b>	<b>49</b>				



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AIR <b>8</b>  NEHANT KUMAR SINGH ME	AIR <b>8</b>  YOGESH KUMAR CE	AIR <b>9</b>  DEEPIITA ROY EE	AIR <b>9</b>  SHUBHAM KARNANI E&T	AIR <b>9</b>  DWEEP SABAPARA ME
AIR <b>9</b>  ANKIT KUMAR CE	AIR <b>10</b>  ANKITA SHARMA EE	AIR <b>10</b>  GAURAV SRIVASTAVA E&T	AIR <b>10</b>  SUMIT BHAMBOO ME	and many more...

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